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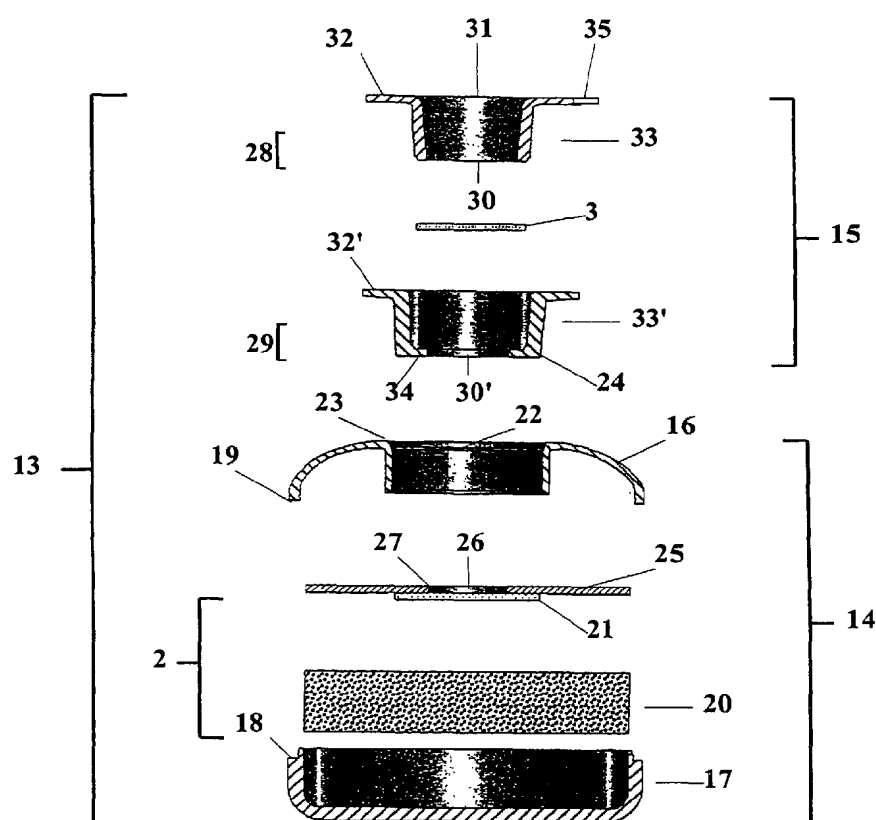
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[Continued on next page]

(54) Title: RAPID VACCINIA ANTIBODY DETECTION DEVICE, METHOD AND TEST KIT



(57) Abstract: A rapid anti-vaccinia virus antibody detection device (13) and method for the detection of anti-vaccinia virus antibodies (10) in a serum, plasma or whole blood test sample (9, 9') utilizing a vaccinia viral lysate (6) as the capture antigen. The detection device (13) operates on the basis of a 2-step flow-through format in use with a multifunctional buffer (12).

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## **RAPID VACCINIA ANTIBODY DETECTION DEVICE, METHOD AND TEST KIT**

### **FIELD OF INVENTION**

5 The invention relates to a rapid vaccinia antibody detection device, method and test kit for the detection of vaccinia antibody in a serum, plasma or whole blood test sample utilizing a purified vaccinia cell lysate as the capture antigen. The detection device operates on the basis of a 2-step flow-through format in use with a push buffer.

### **BACKGROUND OF INVENTION**

10 The global fear of biological warfare has spurred the medical community to implement extra precautionary measures. As a biological weapon, the smallpox virus would pose a serious threat due to its case-fatality rate of 30% or more in unvaccinated persons and to the current unavailability of treatment (Henderson *et al.*, 1999). The waning or non-existent human immunity to the smallpox virus is a great concern in consideration of the fact that the virus has developed a knack for rapid growth in humans, effective spread and persistence.

20 Smallpox may have been used as a biological weapon in North America as early as the mid- to late 1700's when British soldiers initiated outbreaks in Native Americans by distributing blankets that had been used by smallpox patients. Affected tribes lost more than 50% of their population (Henderson *et al.*, 1999) due to the fact that most humans are subject to the ease of transmission and high rate of infectivity of this disease. With Edward Jenner's demonstration of the role of the vaccinia virus' protective abilities against smallpox in 1796, (Henderson *et al.*, 1999; Kaufman *et al.*, 2001), its potential threat of a bioweapon was greatly diminished. The World Health Organization's smallpox eradication campaign, initiated in 1967, saw the last naturally occurring case in the world in Somalia  
30 in 1977 and brought the end to mass vaccinia vaccination programs.

35 The vaccinia virus, a live, animal poxvirus, was a highly effective vaccine responsible for the successful eradication of smallpox over 30 years ago (Kaufman *et al.*, 2001). World-recognized, the vaccinia virus has been safely administered to persons of all ages, providing humans with protective antibodies against smallpox. Although with today's threats, a preventative mass vaccination program will not be possible until increased amounts of vaccine are made available. A recent press release by the United States

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federal government indicates their decision to select pharmaceutical companies to manufacture and stockpile millions of doses of smallpox vaccine in order to protect the American people (Kaufman *et al.*, 2001; Rosenthal *et al.*, 2001). However, the decision to undertake such a massive vaccination program must be weighed against the risk of vaccination complications.

Routine vaccination against smallpox ceased in the United States approximately 30 years ago, leaving today's population highly susceptible to reintroduction of this devastating disease. Statistics show that approximately 114 million people in the United States (42%) are aged 29 years or younger and therefore have not been vaccinated against this disease (Henderson *et al.*, 1999). Furthermore, the immune status of those people who were vaccinated prior to this time is not clear (Rosenthal *et al.*, 2001). The duration of immunity has never been satisfactorily measured but it appears, in general, that a substantial protective antibody decline has been identified during the five to ten year period following smallpox vaccination (Henderson *et al.*, 1999). The underlying strategy in immunizing humans against a particular disease is to prepare an innocuous form of the infectious organism which retains the antigen responsible for establishing protective immunity.

The vaccinia virus vaccine is a live virus from the Poxvirus family which produces defences to smallpox infection in humans. Vaccinia, a eukaryotic virus, reproduces entirely within the cytoplasm of a host cell. It is a lytic virus, i.e. a virus, the replication of which in a cell results in lysis of the cell. The virus is considered non-oncogenic. The virus has been used for approximately 200 years in vaccines for inoculation against smallpox and the medical profession is well acquainted with the properties of the virus when used in a vaccine. Although inoculation with vaccinia is not without risk, the risks are on the whole well known and well defined and the virus is considered relatively benign.

The traditional method for determining success of vaccination against smallpox was simply a qualitative observation of the lesion or scar by a health care professional. Obviously, this method of evaluation is very subjective and requires a vast amount of experience and observation to obtain valid results. A serum neutralization test, process by which serial dilutions of a patient's serum are tested for the presence of antibodies to the vaccinia virus, can be performed to test the ability of the patient sample to neutralize the infectivity of the virus. This technique, however, is very involved and time consuming, taking days to obtain results. On this basis, a more simplistic and rapid approach to the detection of antibodies to vaccinia virus without the aid of complicated instruments and the requisite

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skills and knowledge of professionally trained personnel would be highly desirable. This is especially the case in the event of possible biochemical warfare wherein an emergency response program must be implemented quickly and efficiently to control and prevent possible contamination of the highly infectious disease within a population.

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Accordingly, the present invention provides a rapid vaccinia antibody detection device, method and test kit for the detection of vaccinia antibody in a serum, plasma or whole blood test sample utilizing a purified vaccinia cell lysate as the capture antigen. The detection device, method and push buffer are efficient, reliable and practical to perform. Moreover, the simple design of rapid vaccinia detection device is less costly to manufacture and perform compared to other conventional systems, thus making it more economically feasible and affordable to use. The present invention will be able to provide health professionals a rapid way to monitor the success of the smallpox vaccination process.

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### **SUMMARY OF THE INVENTION**

The rapid vaccinia detection device operates on the basis of a simple 2-step flow-through format in use with a push buffer. The detection device is a dual component flow-through system comprising a test unit in combination with a detachable post-filter unit which are capable of receiving a serum, plasma or whole blood sample and push buffer, respectively. The push buffer serves as a combination washing, diluting, wetting and resolubilizing reagent, without sacrificing the sensitivity or specificity of the test. Additionally, the buffer is formulated to preserve and optimize protein stability, as well as minimize, if not eliminate, non-specific interactions that might lead to the generation of a false signal.

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According to the present invention there is provided a rapid vaccinia antibody detection device, method and test kit for the detection of vaccinia antibody in a serum, plasma or whole blood test sample which utilizes a purified vaccinia cell lysate as the capture antigen. The rapid detection device and method are useful in the detection of protective antibodies for smallpox, which are produced in the human body in response to vaccinia virus vaccination. The rapid vaccinia antibody detection test is designed to be used as a follow-up to vaccination for determination of the success of vaccination, or as a screen test for individuals previously vaccinated during the smallpox eradication program to aid in determination of the requirement for revaccination. Accordingly, the user will be able to determine the success of an individual vaccination, or may be able to indicate the presence or absence of protective antibodies in the serum, plasma or whole blood test sample of an individual vaccinated during the smallpox eradication program 30 or more years ago.

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Using vaccinia viral lysate as a capture antigen, the rapid vaccinia antibody detection test uses flow-through technology consisting of an immunoreactive nitrocellulose membrane, a push buffer and dehydrated gold conjugate cap. A drop of specimen can simply be added to the reactive membrane and the immunocomplex visualized by the addition of a proprietary colloidal gold conjugate colorimetric detection agent.

One of the advantages of the rapid vaccinia antibody detection device and method of the present invention is that it is designed to provide a quick portable, safe and cost-effective method for antibody testing by providing fast and accurate results. It is completely self-contained, requiring no refrigeration for storage or transport and no special equipment other than a standard laboratory centrifuge if a serum/plasma specimen is used. All the reagents and materials required to perform the detection test are provided in a single ready-to-use format. The push buffer provided with the device is a multi-functional reagent which eliminates the potential error for mix-up of reagents during the testing procedure which can lead to erroneous results.

Another advantage of the rapid vaccinia antibody detection device and method is that it provides a qualitative, *in vitro* diagnostic test for the detection of antibodies to the vaccinia virus in human serum, plasma, or whole blood. Accordingly, the rapid vaccinia antibody detection device and method of the present invention is highly effective in qualifying the success of vaccinia vaccination.

The rapid vaccinia antibody detection test utilizes a vaccinia viral lysate coated onto a membrane matrix to capture the antibodies to vaccinia present in human serum, plasma or whole blood when the content of the specimen is placed on the immunoreactive membrane. The captured vaccinia antibodies are visualized through a colorimetric reaction with a colloidal gold-protein A conjugate as the preferred indicator reagent. When the conjugate binds to the vaccinia antibodies, a distinctive horizontal red line appears on the test membrane. A positive test result is obtained when both the red horizontal test line and a red vertical procedural control line are visible at the end of the test procedure. In contrast, a negative result due to the absence of anti-vaccinia virus antibodies is indicated by the presence of only the vertical red procedural control line on the test membrane. If there is no vertical procedural control line present, the test result is invalid.

Using the simplified device and single buffer reagent of the present invention, a qualitative detection test can be performed and read easily, requires a minimum number of steps, does not require lengthy incubation periods, and is highly sensitive, specific and reliable.

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Typically, as little as a single drop (50  $\mu$ L) of a fluid sample is needed to perform the detection test. Moreover, the resulting device and methodology is particularly advantageous in that it is not only convenient and simple to use, but the device and reagents can be stored at room temperature for long periods of time without diminishing the activity or sensitivity of the detection test.

The kinetics of the reaction between the target analyte, i.e. anti-vaccinia virus antibodies, and the indicator reagent are extremely rapid and complete because the detection device and procedure operates on the basis of a flow-through format. Moreover, the method of the present invention improves the accuracy of the detection test compared to conventional assays since the final step of the detection test involves the addition of resolubilized indicator reagent to the test sample after it has previously complexed with the capture reagent, i.e. purified vaccinia viral lysate.

The test unit comprises (1) a reaction zone containing a purified vaccinia viral lysate as the capture reagent that can specifically recognize and bind to antibodies against vaccinia virus, (2) an absorbent zone supporting the reaction zone, and (3) optionally, a blood separation zone contiguous with the reaction zone. The reaction zone of the test unit is oriented so that the label zone of the post-filter unit can be brought into fluid communication therewith after the fluid test sample is applied to the test unit. In a preferred embodiment, the reaction zone is comprised of a porous membrane compatible for immobilization of the capture reagent and has low non-specific binding for the indicator reagent. Any non-specific binding sites on the surface of the porous reaction membrane are inactivated by applying a protein blocking agent. The specificity and affinity of the vaccinia viral lysate immobilized on the reaction membrane allows it to efficiently bind and concentrate any anti-vaccinia virus antibodies contained in a fluid sample within a defined region as the test sample diffuses by capillary action from the reaction membrane to the absorbent zone directly underneath.

To facilitate the detection of anti-vaccinia virus antibodies in a whole blood sample, an alternate embodiment of the present invention provides a test unit capable of receiving and separating the fluid portion of a whole blood sample from the red blood cells (RBC), while transporting the RBC-free fluid portion of the sample to the reaction zone for the detection of the analyte. This particular feature is useful in preventing any interference during visualization of a colour reaction for the detection of anti-vaccinia virus antibodies (i.e. the use of "direct" labels which provide a visually detectable signal without the aid of instruments) and also avoids the necessity to obtain a preliminary extraction of serum or

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plasma in settings where proper equipment to perform such a procedure is unavailable.

Thus, in the case where the fluid sample to be analyzed is a whole blood sample, the test unit optionally features a separate blood separation zone contiguous with the reaction zone. In general, the blood separation zone functions to selectively retain cellular components (i.e. red blood cells) contained within the whole blood sample and deliver the remaining components of the blood sample, including any anti-vaccinia virus antibodies, to the reaction zone. A first end of the blood separation zone, located a short lateral distance from the reaction zone, defines a region for receiving a whole blood sample during the initial stage of the detection test. A second end of the blood separation zone is contiguous with, and thus in direct fluid communication with, the reaction zone thereby promoting the capillary movement of the RBC-free fluid portion of the blood sample from the application zone to the reaction zone for direct detection of the presence of any anti-vaccinia virus antibody. Thus, in effect, the blood separation material functions as a lateral flow material for the selective removal of an effective amount of red blood cells from the whole blood sample to prevent interference with the visual detection of the analyte, while allowing other components of the sample to flow with relatively unimpaired movement through the test unit.

In a preferred embodiment, the blood separation zone is an elongate or rectangular strip of porous material employing a hydrophobic carrier or backing and having intrinsic properties which enable it to preferentially entrap or retain the red blood cells in the sample within the blood separation zone. The carrier or backing provides support for the blood separation material and reduces seepage of the whole blood sample as the RBC-free fluid portion migrates along the material towards the reaction zone.

The second component of the device, namely the post-filter unit, comprises a label zone permeated with a dried indicator reagent and which is capable of being placed in transient fluid communication with the reaction zone of the test unit shortly following application of the test sample to the test unit. Impregnating the label zone of the post-filter unit with a permanently detectable indicator reagent eliminates the need to perform separate resolubilization steps involving precise measuring, adding and premixing with a suitable solvent, thereby increasing the possibility of user error. In a preferred embodiment, the label zone comprises a filter medium selected on the basis of having a pore size large enough so that when the dried indicator reagent is resolubilized by addition of the push buffer, it will easily flow through an exposed area of the porous filter medium by the process of diffusion. The shape and dimensions of the post-filter unit are such that it will



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hold and effectively channel the push buffer through the porous filter medium when the label zone is placed in transient fluid communication with the reaction zone of the test unit during the test procedure.

5 According to another important aspect of the invention, methods and devices are provided utilizing "direct" labeled specific binding materials (i.e. colloidal particle labeled materials) which are dried onto a filter medium and hence, are capable of being rapidly resolubilized and transported to the reaction zone in the presence of the push buffer. Direct labels are well known in the art and highly advantageous for their use in rapid diagnostic systems.

10 Direct labels are capable of producing a visually detectable signal without the aid of instrumentation or the addition of ancillary reagents and are stable when stored in the dry state. Supplying the indicator reagent by way of incorporating it within the filter medium in a dried form provides an inexpensive and convenient means of storing such reagent. The preferred label for carrying out diagnostic assays is colloidal metal particles, more

15 preferably colloidal gold, although other direct labels may be employed which include, but are not limited to, non-metal sols, dye sols, latex particles, carbon sol, and liposome contained colored bodies.

According to a further important aspect of the present invention, there is provided a push

20 buffer in the detection test which does not require ancillary additives, or the maintenance and inspection by laboratory instruments. More importantly, however, is the multifunctional nature of the push buffer which enables it to serve as a combination wash solution, diluent, resolubilization and solvent transport reagent, thereby eliminating the need for several separate solutions and steps to be performed during the detection test

25 protocol. The multifunctional nature of the push buffer greatly simplifies the detection test procedure by reducing the time and manual steps required to perform the test, thereby minimizing the likelihood for user error. In addition, utilizing the push buffer in a flow-through format promotes quick release and enhanced mass transfer of the dried indicator reagent from the post-filter unit to the test unit immediately following resolubilization.

30 Other functional properties exhibited by the push buffer are that it maintains protein stability, thereby preserving and optimizing the specific binding reaction that occurs between complementary binding members, i.e. capture reagent and target analyte. Moreover, upon resolubilization of the dried indicator reagent, the push buffer helps to optimize signal generation in the case of a specific binding reaction and minimize

35 nonspecific binding to the reaction membrane that might otherwise lead to the generation of a false signal.

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According to yet a further aspect of the present invention, there is provided a simple 2-step procedure for performing the rapid vaccinia antibody detection method comprising (1) depositing a fluid test sample onto the reaction zone of the test unit, or if a whole blood sample, onto a first end of a blood separation zone, shortly thereafter bringing the test unit and the post-filter unit into operable association such that the label zone of the post-filter unit is in transient fluid communication with the reaction zone of the test unit, and (2) adding the push buffer to the post-filter unit followed by removal of the post-filter unit to observe the test result. Following addition of the push buffer to the post-filter unit, the buffer diffuses through the label zone to reconstitute the indicator reagent and transport it to the reaction zone where it will bind with any captured anti-vaccinia virus antibody. If anti-vaccinia virus antibody is present in the fluid sample, a detectable signal will appear in the reaction zone which can be visually inspected for color and thus, a determination of the presence or absence of anti-vaccinia virus antibody made following removal of the post-filter unit.

The present invention also provides a rapid vaccinia antibody detection test kit for use in the determining whether there is any anti-vaccinia antibody in a fluid test sample. Essentially, the kit comprises in a packaged combination: the rapid vaccinia antibody detection device comprising both the test unit and post-filter unit as described above; a push buffer for reconstitution of the dried indicator reagent; and instructions for performing the detection test. The test kit preferably includes a suitable container for housing the test unit and the post-filter unit in order to safeguard the solid phase materials and dried indicator reagent from contamination, as well as to provide ease and convenience in handling of the detection test device. Optionally, the test kit also includes a means for applying the test sample and push buffer to the test unit and post-filter unit, respectively (e.g. disposable pipettes).

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1A is a diagrammatic illustration of a test sample applied to the porous reaction membrane of the test unit which contains anti-vaccinia virus antibody;

Fig. 1B is a diagrammatic illustration of the anti-vaccinia virus antibody complexed with vaccinia viral lysate as the capture reagent after the test sample has completely diffused through the reaction membrane and into the absorbent material of the test unit;

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Fig. 1C is a diagrammatic illustration of the post-filter unit in fluid communication with the reaction membrane of the test unit, to which the push buffer is added;

Fig. 1D is a diagrammatic illustration of resolubilized indicator reagent reacted with complexed vaccinia viral lysate and anti-vaccinia virus antibody following addition of the push buffer to the post-filter unit;

Fig. 2A is a diagrammatic illustration of a test sample applied to the porous reaction membrane of the test unit which does not contain anti-vaccinia virus antibody;

Fig. 2B is a diagrammatic illustration of uncomplexed vaccinia viral lysate as the capture reagent after the test sample has diffused through the reaction membrane and into the absorbent material of the test unit;

Fig. 2C is a diagrammatic illustration of the post-filter unit in fluid communication with the reaction membrane of the test unit, to which the push buffer is added;

Fig. 2D is a diagrammatic illustration of unreacted indicator reagent following resolubilization by the push buffer after diffusing through the reaction membrane and into the absorbent material of the test unit;

Fig. 3 shows an exploded cross-sectional view of a preferred embodiment of a suitable container which houses the test unit and the post-filter unit; and

Fig. 4 shows an enlarged cross-sectional view of the container of Fig. 4 in its assembled form;

Fig. 5 is a diagrammatic illustration of a second embodiment of a portion of the test unit comprising a material defining the blood separation zone in fluid communication with the reaction zone; and

Figs. 6A and 6B are a diagrammatic illustration of top plan views of the top and bottom members of a 2-reservoir test cartridge for receiving and analyzing a whole blood sample.

While this invention is satisfied by embodiments in many different forms, there will herein be described in detail preferred embodiments of the invention, with the understanding that the present disclosure is to be considered as exemplary of the principles of the invention

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and is not intended to limit the invention to the embodiments illustrated and described. The scope of the invention will be measured by the appended claims and their equivalents.

### DETAILED DESCRIPTION

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Unless defined otherwise, all technical and scientific terms used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. As employed throughout the disclosure, the following terms, unless otherwise indicated, shall be understood to have the following meanings.

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It must also be noted that, as used in the specification, the singular forms "a," "an" and "the" include plural referents unless the context clearly dictates otherwise. Ranges may be expressed herein as from "about" or "approximately" one particular value and/or to "about" or "approximately" another particular value. When such a range is expressed, another embodiment includes from the one particular value and/or to the other particular value. Similarly, when values are expressed as approximations, by use of the antecedent "about," it will be understood that the particular value forms another embodiment.

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**Capillary Action** - as used herein, the term "capillary" includes a capillary or other channel or pathway which permits a liquid to traverse the absorbent material of the invention. The absorbent material is in capillary communication with the reaction membrane of the test unit and is selected to have a capillary pore size so as to induce flow of liquid through the reaction membrane without the use of external means when the hydrostatic pressure of the sample and subsequent addends used in the detection test are not sufficient to induce flow through the reaction membrane. The absorbent material may also provide support for the reaction membrane.

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**Fluid Sample** - the fluid sample is tested to form a detectible reaction product on the reaction membrane of the test unit. In preferred embodiments of the detection test, the fluid sample is biologically derived (e.g. whole blood, plasma, serum, urine, saliva, etc.) and is suspected to include as the target analyte, anti-vaccinia virus antibody capable of being bound by the vaccinia viral lystate immobilized on the reaction membrane as the capture reagent.

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**Indicator Reagent** - a conjugate comprised of a specific binding member to the anti-vaccinia virus antibody and a label that is capable of being visually detected. A preferred indicator reagent of the present invention is protein A labeled with colloidal gold. Other

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indicator reagents for anti-vaccinia virus antibody as the target analyte would include, for example, goat antihuman IgG labeled with colloidal gold.

**Label** - a label may be any molecule bound or conjugated to a specific binding member which can produce a signal. In the subject invention, the label is preferably a "direct" label which is capable of spontaneously producing a detectible signal without the addition of ancillary reagents and will be easily detected by visual means without the aid of instruments. The preferred embodiment of the invention uses colloidal gold particles as the label. Other suitable labels may include other types of colloidal metal particles, minute colored particles, such as dye sols, and coloured latex particles. Many such substances will be well known to those skilled in the art.

**Solid Phase** - methods have also been developed for carrying out "solid phase" assays wherein immunological reactions are carried out in solution on solid substrates including those which are porous or fibrous materials. According to such procedures, porous carrier materials are fashioned into strips or other forms to which the capture reagent, e.g. antibodies, antigens) are immobilized by adsorption, absorption or covalent bonding.

In a preferred embodiment of the invention, the type of method employed is based on an immunofiltration dotting assay system for the purposes of convenience and utility wherein components of a vaccinia viral lysate have been immobilized onto a solid support to effect a reaction. Immunofiltration dotting techniques are well known in the art.

## 1.0 INTRODUCTION

The detection device useful in the practice of the invention is a dual component flow-through system comprising a test unit and a post-filter unit capable of receiving the fluid sample and push buffer, respectively. The test unit comprises a reaction zone containing purified vaccinia viral lysate that can specifically bind with anti-vaccinia virus antibody, an absorbent zone supporting the reaction zone, and optionally, a blood separation zone contiguous with the reaction zone. The reaction zone of the test unit is oriented so that the label zone of the post-filter unit can be brought into transient fluid communication therewith shortly after the fluid test sample is applied to the reaction zone of the test unit. To facilitate the detection of anti-vaccinia virus antibody in a whole blood sample, an alternate embodiment of the present invention provides a test unit further comprising a blood separation zone contiguous with the reaction zone, whereby a first end of the blood separation zone located a short lateral distance from the reaction zone defines a region for

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receiving the whole blood sample. A second end of the blood separation zone slightly overlaps with the reaction zone so as to be in direct fluid communication therewith. The post-filter unit comprises a label zone containing a dried indicator reagent and is capable of being placed in transient fluid communication with the reaction zone of the test unit during the detection test procedure.

The detection test protocol is a simple 2-step procedure involving (1) depositing a fluid test sample onto the reaction zone of the test unit, or if a whole blood sample, onto a first end of the blood separation zone, shortly thereafter bringing the test unit and the post-filter unit into operable association such that the label zone of the post-filter unit is in transient fluid communication with the reaction zone of the test unit, and (2) adding the push buffer to the post-filter unit and removing the post-filter unit to observe the test result. The push buffer passively diffuses through the label zone of the post-filter unit to resolubilize the indicator reagent and transport it to the reaction zone of the test unit where it will bind to anti-vaccinia virus antibody that has complexed with the vaccinia viral lysate. If anti-vaccinia virus antibody is present in the fluid sample, a detectable signal will appear in the reaction zone which can be easily visualized following removal of the post-filter unit from the test unit. An advantage provided by the methodology of the present invention is the enhanced sensitivity and reliability of the test. This is achieved by maximizing the opportunity for thorough capture of the analyte, even at low concentrations, and avoiding the implementation of method steps which increase the likelihood of contamination of the sample and reagents.

## 2.0 SANDWICH TECHNIQUE

Figure 1 is a diagrammatical illustration showing the method of the invention using the rapid vaccinia antibody detection device. In this particular instance, Figure 1A shows a fluid test sample **9** containing anti-vaccinia virus antibody **10**, as well as other non-essential components **11**, which is applied to the reaction zone **5** of the test unit **2**. As the fluid sample **9** diffuses through the reaction zone **5** and into the absorbent zone **4** underneath, the free anti-vaccinia virus antibody **10** comes into contact with components of the vaccinia viral lysate **6** and forms a complex, while unbound non-essential component **11** continues to be drawn into the absorbent zone **4** below (Figure 1B). As shown in Figure 1C, the label zone **7** of the post-filter unit **3** is subsequently brought into fluid communication with the reaction zone **5** of the test unit **2** prior to the addition of the push buffer **12**. Immediately following resolubilization of the dried indicator reagent **8** by the buffer **12**, the indicator reagent **8** is transported to the reaction zone **5** of the test unit **2**,

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where it will bind with any anti-vaccinia antibody **10** that has complexed with components of the vaccinia viral lysate **6**. The binding reaction of the indicator reagent **8** with anti-vaccinia virus antibody **10** produces a visually detectable signal thereby indicating a positive reaction that is easily observed following removal of the post-filter unit **3**, as per Figure 1D.

Figure 2A is a diagrammatical illustration showing the method of the invention using the rapid vaccinia antibody device when a fluid test sample **9** devoid of anti-vaccinia virus antibody is applied to the reaction zone **5** of the test unit **2**. As the fluid sample **9** diffuses through the reaction zone **5** and into the absorbent zone **4** underneath, the non-essential components **11** completely bypass the components of the vaccinia viral lysate **6** (Figure 2B). As shown in Figure 2C, the label zone **7** of the post-filter unit **3** is subsequently brought into fluid communication with the reaction zone **5** of the test unit **2** prior to the addition of the push buffer **12**. Immediately following resolubilization of the dried indicator reagent **8** by the buffer **12**, the indicator reagent **8** is transported to the test unit **2**, where it diffuses through the reaction zone **5**, pass the components of the vaccinia viral lysate **6** and into the absorbent zone **4** below due to the absence of any anti-vaccinia virus antibody complexed with the lysate **6**. Following removal of the post-filter unit **3**, a color signal will not be detected thereby indicating a negative result due to the absence of binding between the indicator reagent **8** and complexed anti-vaccinia virus antibody.

To facilitate the detection of a target analyte in a whole blood sample, an alternate embodiment of the present invention provides a test unit having a blood separation zone capable of receiving and separating the fluid portion of a whole blood sample from the red blood cells (RBC), while transporting the RBC-free fluid portion, including any analyte, to the reaction zone for direct analysis. As shown in Figure 5, the blood separation zone **100** is preferably an elongate or rectangular strip of porous material employing a hydrophobic carrier **103**. The preferred material for the blood separation zone **100** is selected on the basis of having intrinsic properties which enable it to preferentially entrap or retain the red blood cells in the sample **9'** as the fluid portion migrates in a lateral direction towards the reaction zone **5**. Although the shape and dimensions are not critical, preferably the blood separation zone **100** is a rectangular form having dimensions suitable for allowing efficient removal of a substantial amount of red blood cells from the whole blood sample **9'** prior to the RBC-free fluid portion of the sample **9'** arriving at the reaction zone **5**. Thus, in effect, the blood separation material functions as a lateral flow material for the selective removal of an effective amount of red blood cells from the whole blood sample **9'** so as to avoid interference with the visual detection of the analyte, while allowing other

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components of the sample, including any analyte, to flow with relatively unimpaired movement to the reaction zone **5**.

A first end **101** of the blood separation zone **100**, located a short lateral distance from the reaction zone **5**, defines a region for receiving the whole blood sample **9'** during the initial stage of the detection test protocol. A second end **102** of the blood separation zone **100** is contiguous with and overlaps slightly with the reaction zone **5**, so as to be in direct fluid communication with the reaction zone **5**, thereby promoting the capillary movement of the RBC-free fluid portion of the blood sample **9'** from the first end of the blood separation zone **100** to the reaction zone **5**. The blood separation zone **100** and the reaction zone **5** must contact one another in order to ensure optimal transfer of the sample from one zone to the other. Therefore, it is preferably that the blood separation zone **100** and the reaction zone **5** overlap with one another slightly as opposed to being abutted to one another.

The hydrophobic carrier **103** affixed to the lower surface of the blood separation zone **100** provides support and reduces seepage of the fluid phase while the RBC-free fluid portion of the whole blood sample migrates towards the reaction zone **5**. Suitable materials for use as a carrier **103** include, for example, polycarbonate, polyethylene, Mylar, polypropylene, vinyl, cellophane and polystyrene, etc. as well as water-proofed or water-resistant cardboard or similar materials. The carrier **103** may be affixed either directly or indirectly to the blood separation material by means of an adhesive. The carrier **103** is preferably similar in shape and size to the blood separation zone **100**.

Thus, the two-step method protocol optionally employs a simultaneous separation of red blood cells from a whole blood sample **9'** in order to permit testing for anti-vaccinia virus antibody without the requirement for additional steps. For example, in the case where a whole blood sample **9'** contains anti-vaccinia virus antibody, the sample **9'** is simply applied to the first end of the blood separation zone **100** of the test unit **2**, rather than the reaction zone **5**. As the RBC-free fluid portion of the blood sample **9'** migrates in a lateral direction to arrive at the reaction zone **5**, the free anti-vaccinia virus antibody **10** eventually comes into contact with components of the vaccinia viral lysate **6** and forms a complex. Thus, similar to the method step shown in Figure 2B, unbound non-essential components **11** are drawn into the absorbent zone **4** located beneath the reaction zone **5**. The label zone **7** of the post-filter unit **3** is subsequently brought into fluid communication with the reaction zone **5** of the test unit **2** prior to the addition of the push buffer **12** (refer to Figure 1C). Immediately following resolubilization of the dried indicator reagent **8** by



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### 3.0 TEST UNIT

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### 3.1 REACTION ZONE

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particles in the separation step of the detection test can be facilitated by the addition of a fibrous or hydrophilic material (absorbent pad) in contact with the underside of the porous reaction membrane. The size of the area exposed to the solid phase particles can be controlled by using a device comprised of a hydrophobic material such as plastic, plastic laminate, or other similar substance that is placed in contact with the porous film and seals the porous reaction membrane such that only a surface area no greater than 150 mm<sup>2</sup> is exposed to the particulate solid phase.

Another factor to be considered is that the material of the porous reaction membrane be selected on the basis that it is compatible for immobilization of the vaccinia viral lysate. The reaction membrane may be any suitable porous material so long as the performance of the detection test is not adversely affected. Suitable materials include nitrocellulose (supported or unsupported), glass fiber, polyester, cellulose nitrate, polyester, polycarbon, nylon, and other natural and synthetic materials which can be coupled directly or indirectly to components of the vaccinia viral lysate. Some of these materials may comprise negative charges to assist in immobilization, such as cellulose nitrate which has partial negative charges contributed by the nitro groups.

In some cases commercial filters are available that have immobilized to their internal and/or external surfaces a reactant for the attachment of biological molecules, such as antibodies or antigens, to the surfaces. Examples of various filters include cellulosic filters (filter papers), polyamide membranes (e.g. numerous variations of polyamide membranes are manufactured by the Pall Corporation), and various other microporous membranes, such as those available commercially from Amicon, Geleman, and Schleicher & Schuell. For example, the following membranes are available from Pall Corporation: Biodyne®, a N66 polyamide microporous membrane (U.S. Patent No. 4,340,479 issued to Pall); Carboxydyne®, a hydrophilic, microporous, skinless nylon 66 membrane with control surface properties characterized by carboxyl functional groups at its surfaces; and Immunodyne™, a modified Carboxydyne® membrane prepared by treating a Carboxydyne® membrane with trichloro-s-triazine. Other microporous membranes, prepared by the Millipore Corporation, are described in U.S. Patents Nos. 4,066,512 and 4,246,339.

Other materials may be pre-treated to provide a charged membrane. For example, polyester can be derivatized with carboxyl or amino groups to provide either a negatively or positively charged membrane. Nylon can be treated with acid to break peptide bonds to provide positive charges (from the amine groups) and negative charges (from the

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carboxyl groups).

The porosity of the membrane has a large influence on the flow rate of the liquid and sensitivity of the detection test. The larger the pore size of the membrane, the faster the flow rate for a given liquid. As the flow rate increases, the interaction time available between the target molecule in the sample and the receptor immobilized on the reaction membrane decreases, thus decreasing detection test sensitivity. Additionally, larger pore sizes provide less surface area for immobilizing the receptor molecule, which is another parameter attributable to decreased detection test sensitivity. For the detection device of the present invention, the porosity of the membrane is preferably in the range of about 0.1 to about 12 microns, and more preferably about 0.45 to 3 microns. The porosity of the membrane preferably varies from about 0.2 to about 12 microns.

The wicking power of the membrane may also affect detection test sensitivity and depends on the thickness and nature of the membrane material. Wicking power can be measured as the migration of a standard solution through a certain distance per unit time. Often times, selecting a membrane having a relatively low wicking power can increase detection test sensitivity. In addition to porosity, the diameter and thickness of the reaction membrane may affect detection test sensitivity and therefore, must be considered. The depth or thickness of the membrane is selected so that an adequate amount of vaccinia viral lysate can be immobilized to capture the anti-vaccinia virus antibody. However, the thickness should not be so great as to cause undue delay of the passage of the fluid sample through the membrane.

The thickness of the reaction membrane, which is the distance between the upper and lower surfaces of the reaction membrane will range from about 0.05 mm to about 3.0 mm, and more commonly from about 0.1 to about 1.0 mm. It has been found that when the thickness of the reaction membrane is greater than about 0.1 mm, and preferably in the range of about 0.2 mm to about 1.0 mm, higher sensitivity can be achieved. Additionally, a thicker reaction membrane may allow more vaccinia viral lysate to be available for binding to anti-vaccinia virus antibody, thereby providing a further increase in detection test sensitivity. It is believed that prior art devices which have relatively thin reaction membranes, such as nitrocellulose membranes less than 0.1 mm thick which are not paper-backed, tend to allow the sample to flow sideways across the reaction membrane rather than downwards through the middle of the reaction membrane.

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However, as a presently preferred embodiment, the reaction membrane comprises paper-backed nitrocellulose, or other types of nitrocellulose membranes with similar characteristics. The preferred embodiment of the present invention comprises a nitrocellulose membrane backed with porous paper similar to filter paper. A representative  
5 example is commercially available under the trade name BAC-T-KOTE by Schleicher and Schuell. This preferred membrane is substantially more durable than nitrocellulose alone and can be employed without any other support component. Also, it provides enhanced sensitivity to the reaction. Also, polyester supported nitrocellulose may be used such as supplied under the name NITROPLUS by Micron Separation, Inc.

10 The term "reaction zone" is intended to include the porous material to which the vaccinia viral lysate and other molecules employed in the detection test are bound as well as additional porous supporting material, if any, that forms the lower surface of the reaction zone. For example, a preferred reaction zone comprises a sheet of nitrocellulose backed  
15 with a porous paper. Commercially available porous polyester supported nitrocellulose can also be used. A representative example of paper-backed nitrocellulose is commercially available from EY Laboratories Inc. (San Mateo, Calif.; Cat. Nos. PBNC15-1, PBNC15-10, PBNC15M-1, and PBNC15M-10). This preferred material is substantially more durable than nitrocellulose alone and can be employed without any other support component. This  
20 allows for easier handling and device assembly. Additionally, it has been found that detection devices employing paper-backed nitrocellulose for the reaction zone have enhanced sensitivity in most instances.

### 3.2 IMMOBILIZATION OF THE CAPTURE REAGENT

25 In a typical system, the vaccinia viral lysate is immobilized on the porous membrane of the reaction zone which will specifically bind to any anti-vaccinia virus antibody present in the fluid sample being screened. The vaccinia viral lysate can be immobilized directly or indirectly onto such materials, such as nitrocellulose, by either absorption, adsorption, or  
30 covalent bonding. When a test sample suspected of containing anti-vaccinia antibody is applied to the reaction zone containing the immobilized vaccinia viral lysate, it becomes non-diffusively bound to the reaction zone. Thus, by appropriate application of a fluid sample suspected of containing anti-vaccinia antibody, a high concentration of the target analyte can be obtained in a well defined region within the center of the reaction zone. In  
35 appropriate cases, the vaccinia viral lysate may be coated on the upper surface of the reaction zone or entrapped within the matrix of the porous material of the reaction zone. Therefore, as used herein, the term "immobilized" is intended to embrace any means for

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fixing the capture reagent to the porous material.

A first step of the present method is to immobilize the capture reagent within a finite zone of the reaction zone. Immobilization can be accomplished by methods such as adsorption, absorption, evaporative deposition from a volatile solvent solution, covalent bonding  
5 between the capture reagent and the reaction membrane, or immunological immobilization. Covalent bonding may, for example, involve bonding the capture reagent to the reaction zone through a coupling agent, such as a cyanogen halide, e.g. cyanogen bromide or by the use of gluteraldehyde, as described by Grubb, et al. in U.S. Patent No. 4,186,146.  
10 Immunological immobilization to the reaction membrane may be by absorption, or by covalent linkage, directly, or through a linker of sorts well-known to those skilled in the art. Suitable methods of carrying out these procedures are given, for example, by Iman and Hornby in Biochemical Journal (Volume 129; Page 255; Campbell, Hornby, and Morris in Biochem. Biophys. Acta (1975), Volume 384; Page 307; and Mattisson and Nilsson in  
15 F.E.B.S. letters, (1977) Volume 104, Page 78. See also, for example, U.S. Patents Nos. 4,376,110 and 4,452,901. In addition, chemically pretreated materials suitable for coupling antibodies can be purchased commercially.

Immunological immobilization is preferred for the practice of the present invention wherein  
20 the porous reaction membrane is impregnated with a vaccinia viral lysate by way of absorption using a dispenser/printer technique (BioDot, California, USA). The technique essentially involves applying the lysate to the membrane by spraying it directly onto a porous reaction membrane. The above technique is most readily achieved using a commercial printing device termed a BIOJET QUANTI 3000, and provides a stream of the  
25 capture reagent under a variety of conditions, and at varying stream widths. Using this technique, it is possible to rapidly deposit a series of lines, or other discrete patterns on the reaction membrane. Preferably, the vaccinia viral lysate is deposited in a discrete test zone having an area substantially smaller than that of the entire surface area of the porous material. In addition, it is preferred that the pattern is in the form of a single discreet line  
30 to enhance the visibility of the result.

### 3.3 CONTROL ZONE

In addition to the capture reagent, a defined area of the exposed reaction zone may also  
35 contain a control molecule. In this regard, color development at the test site may be compared with the color of one or more standards controls to determine whether the reagents are stable and the test is performing properly. In general, when testing for the

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presence of anti-vaccinia antibody, the detection device will have a built-in control of an antibody directed to human immunoglobulin G (IgG), IgM, IgE, or IgA. Thus when a fluid test sample (e.g. plasma or serum) is added to the diagnostic device, immunoglobulin will bind to the control region regardless of whether or not analyte happens to be present in the sample. For example, a suitable control may be established by using Protein A which is disclosed in U.S. Patent No. 5,541,059 (Chu). Other suitable controls are well known in the art.

### 3.4 BLOCKING THE REACTION ZONE

As noted above, the vaccinia viral lysate, and the optional use of controls, are typically applied only to defined regions of the exposed surface of the reaction zone. The vaccinia viral lysate will be applied to a defined region within the center of the reaction zone such that the perimeter of the exposed surface of the reaction zone will not have any lysate bound thereto. In this regard, the remainder of the porous material or membrane from which the zone is made can be treated with a blocking composition that prevents the target substance and other components of the sample from non-specifically binding to the reaction zone. The use of a good quality paper-backed nitrocellulose may make a blocking step unnecessary in some assays. However, if a blocking step is needed, a common blocking solutions comprising bovine serum albumin (BSA) or other proteins which do not interfere with or cross-react with reagent materials of the detection test can be used. BSA is usually used in amounts from about 1 to 10%.

The blocking treatment typically occurs after the detection device has already been assembled and the vaccinia viral lysate is immobilized to the reaction zone. A sufficient amount of blocking composition which will cover the exposed surface of the reaction zone is applied. After the blocking composition has dried, the detection device is ready for use.

### 3.5 ABSORBENT ZONE

The sensitivity of reaction-membrane type immunoassays (i.e. the ability to detect very low levels of target substance) can be increased if the sample is concentrated through the reaction zone. With some devices, concentration of the sample through a reaction zone is achieved by having an absorbent material, or pad, beneath the reaction zone that draws the sample, which is added to the surface of the reaction zone, through to the absorbent material below. The absorbent zone can be generated from any material capable of wicking fluid by way of capillary action, such as cotton or paper. Membrane-based

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immunoassays that utilize various absorbent materials to concentrate sample are exemplified in U.S. Patents Nos. 5,185,127, 5,006,464, 4,818,677, 4,632,901, and 3,888,629.

5 An absorbent material is situated underneath the lower surface of the reaction zone so as to be in direct fluid communication with the reaction zone. Thus, the upper surface of the absorbent material is immediately adjacent to the lower surface of the reaction zone. Fluid communication contact involving direct physical contact of the absorbent material with the reaction zone may include the separation of a portion of the absorbent material from the  
10 reaction zone by an intervening spacer layer, thereby essentially defining a test zone. Although not critical to the performance of the apparatus, the spacer layer also serves to hold the porous membrane of the reaction zone and permit detection test reagents to flow uniformly from the upper surface down to the lower surface of the detection test apparatus. The spacer layer may be made of any rigid or semi-rigid porous material that  
15 does not bind or interact with detection test reagents used in conjunction with the invention. In embodiments of the invention where ease of manufacture and reduced costs are desired, the upper surface of the absorbent material is typically immediately adjacent the lower surface of the reaction zone.

20 The selection of material for the absorbent zone is not critical and a variety of fibrous filter materials can be used, including one or more layers of the same or different materials, providing that the material selected is compatible with the analyte and the detection test reagents. Any conventionally employed absorbent material that is capable of drawing or wicking fluid through a porous membrane, such as for example, by capillary action, can be  
25 used in the present invention. The absorbent material should be capable of absorbing a volume of fluid sample that is equivalent or greater than the total volume capacity of the material itself. Useful known materials include cellulose acetate fibers, polyester, polyolefin or other such materials. The absorbent material provides a means to collect the sample by providing uniform "suction" to deliver the sample from the well, through the  
30 reaction zone, and down into the absorbent material. Thus, the absorbent body also acts as a reservoir to hold the sample, and various reagents that are used when the detection test is performed. Accordingly, when used in tests where relatively large volumes of fluid are used, the absorbent material should have high absorbent capacity so as to prevent or minimize the possibility of back-flow of sample and reagents from the absorbent body back  
35 into the reaction membrane.

As with the reaction zone material, the wicking power of the absorbent material can be an

important parameter. Wicking time is defined in terms of the time required for water to travel a defined distance through the absorbent paper and is related to the basis weight, thickness, and composition of the paper. Wicking power can vary greatly from one material to the next. Thus, the properties of the analytical device and flow rate of sample and reagents can be modified by varying the absorbent material used.

### 3.6 BLOOD SEPARATION ZONE

To facilitate the detection of anti-vaccinia virus antibody in a whole blood sample, an alternate embodiment of the present invention provides a test unit capable of receiving and separating the fluid portion of a whole blood sample from the red blood cells (RBC) featuring a blood separation zone contiguous with the reaction zone. The blood separation zone functions to selectively retain cellular components (i.e. red blood cells) contained within the whole blood sample and deliver the remaining components of the RBC-free fluid portion of the blood sample, including any anti-vaccinia virus antibody, to the reaction zone for eventual analysis. This particular feature is useful in preventing any interference during visualization of a color reaction for the detection of anti-vaccinia virus antibody and avoids the necessity of obtaining a preliminary extraction of serum or plasma in settings where proper equipment to perform such a procedure is unavailable.

Various methods for the separation of blood cells from the fluid portion of blood are described using separation coatings, erythrocyte aggregating and agglutinating agents, materials having asymmetric pore sizes, polymer-containing matrixes, and multilayer systems, to name a few, e.g. U.S. Pat. No. 3,768,978 to Grubb et al., U.S. Pat. No. 3,902,964 to Greenspan, U.S. Pat. No. 4,477,575 to Vogel et al., U.S. Pat. No. 4,594,372 to Zuk, U.S. Pat. No. 4,753,776 to Hillman et al., U.S. Pat. No. 4,816,224 to Vogel et al., U.S. Pat. No. 4,933,092 to Aunet et al., U.S. Pat. No. 5,055,195 to Trasch et al., U.S. Pat. No. 5,064,541 to Jeng et al., U.S. Pat. No. 5,076,925 to Roesink et al., U.S. Pat. No. 5,118,428 to Sand et al., U.S. Pat. No. 5,118,472 to Tanaka et al., U.S. Pat. No. 5,130,258 to Makino et al., U.S. Pat. No. 5,135,719 to Hillman et al., U.S. Pat. No. 5,209,904 to Forney et al., U.S. Pat. No. 5,212,060 to Maddox et al., U.S. Pat. No. 5,240,862 to Koenhen et al., U.S. Pat. No. 5,262,067 to Wilk et al., U.S. Pat. No. 5,306,623 to Kiser et al., U.S. Pat. No. 5,364,533 to Ogura et al., and U.S. Pat. No. 5,397,479 to Kass et al..

In a preferred embodiment, the blood separation zone is an elongate or rectangular strip of porous material having intrinsic physical properties which enable it to preferentially and sufficiently entrap or retain the red blood cells in the sample within the blood separation



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zone. A first end of the blood separation zone located a short lateral distance from the reaction zone, defines a region for receiving the whole blood sample during the initial stage of the detection test. A second end of the blood separation zone overlaps slightly with the reaction zone, so that it is in direct fluid communication with the reaction zone, thereby promoting the movement of the RBC-free fluid portion of the blood sample from the first end of the blood separation zone to the reaction zone for eventual analysis. The blood separation zone and the reaction zone must contact one another in order to ensure optimal transfer of the sample from one zone to the other.

A variety of materials can be used for the blood separation zone such as glass fiber, glass fiber/cellulose mixtures, cellulose, or other proprietary materials, including synthetic materials, e.g., nylon. Preferably, a permeable glass fiber matrix is employed as the blood separation material to facilitate the separation of red blood cells from whole blood. A variety of grades of different thicknesses and absorbencies of glass fiber materials are commercially available to facilitate blood separation and include, for example, GF-24, GF-25, and #33, available from Schleicher & Schuell (Keene, N.H., USA); G143, G144, and G167, available from Ahlstrom (Mount Holly Springs, Pa., USA); GFQA30VA, GF/P 30, GF/DE 30, GF/SE 30, GF/CM30VA, GF/CM 30, F 075-14, F487-09, GF DVA, GFVA 20, and GD-2, available from Whatman (Fairfield, N.J., USA).

Useful glass fiber/cellulose mixture materials include F255-07 90 glass/10 cellulose, F255-09 70 glass/30 cellulose, F255-11 50 glass/50 cellulose, and F255-12 50 glass/50 cellulose, available from Whatman.

Useful cellulose materials include 598, available from Schleicher & Schuell. Miscellaneous or other materials falling outside the above categories can also be used, including HemaSep V and Leukosorb; which article of manufacture according to the subject invention available from Pall BioSupport (Port Washington, N.Y., USA).

One useful nylon material is Nylon 6.6 Transfer Membrane, which is commercially available under the tradename Biodyne B (Pall Specialty Materials, Port Washington, N.Y.). In addition, the material known as "PlasmaSep", available from Whatman, can be used.

Although the shape and dimensions of the blood separation zone are not critical, preferably it has a narrow rectangular form and dimensions suitable for allowing efficient removal of a substantial amount of red blood cells from the whole blood sample during migration of

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the fluid portion of the sample from the first end to the second end of the zone. Thus, in effect, while a narrow rectangular shape is preferred to channel fluid portion of the blood sample to the reaction zone, the dimensions may vary depending on the intrinsic properties (e.g. absorbency, migration rate, etc.) of the material selected for the blood separation zone. In a preferred embodiment, the blood separation zone is made using the glass fiber material F487-09, available from Whatman, having dimensions between about 4 and 7 mm in width, between about 10 and 15 mm in length, and between about 0.2 mm and 1.0 mm in thickness. More preferably, the blood separation material is about 7 mm in width by about 10 mm in length and about 0.5 mm in thickness. These dimensions are optimized to be capable of receiving and separating the total volume of a whole blood sample, e.g. two drops of blood.

The blood separation material preferably has a rigid or semi-rigid carrier or backing affixed to its lower surface to provide support and reduce seepage of the RBC-free fluid portion of the whole blood sample while it migrates towards the reaction zone. Suitable materials for use as a carrier or backing include, for example, hydrophobic materials such as polycarbonate, polyethylene, Mylar, polypropylene, vinyl, cellophane and polystyrene, etc. as well as water-proofed or water-resistant cardboard or similar materials. The carrier or backing may be affixed either directly or indirectly to the blood separation material by means of an adhesive. Suitable adhesives are well-known in the art. The carrier may be of any shape and of almost any size which may conveniently be handled. However, the carrier is preferably similar in shape and size to the blood separation material. In a preferred embodiment, the carrier is formed as an elongate or rectangular strip having a length and width similar to or the same as the blood separation material.

#### 4.0 POST-FILTER UNIT

As discussed above, the diagnostic device of the present invention comprises, as a second member, a post-filter unit comprising a label zone permeated with a dried indicator reagent.

The selection of the material for the label zone is not critical and can be any suitably absorbent, porous or capillary possessing material through which the push buffer and resolubilized indicator reagent may be transported by wicking action. The criteria of selection is that the material allow for the resolubilization and mixing of the dried indicator reagent upon addition of the push buffer, as well as initiate the transfer of the buffer and freshly dissolved indicator reagent to the reaction zone of the test unit.

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Natural, synthetic, or naturally occurring materials that are synthetically modified, can be used as a filter medium including, but not limited to: cellulose materials such as paper, cellulose, and cellulose derivatives such as cellulose acetate and nitrocellulose, fiberglass, cloth, films of polyvinyl chloride, and the like. A preferred filter medium is nitrocellulose, however, the material should be chosen for its ability to premix the push buffer with the resolubilized indicator reagent. Moreover, the fluid flow through the filter medium should be laminar as opposed to turbulent flow characteristics which allows the initial mixing of the buffer with the indicator reagent. If nitrocellulose is used as the filter medium, then a preferred material is glass fiber filter paper because it enables the mixing and transfer of resolubilized indicator reagent to the reaction membrane.

#### 4.1 INDICATOR REAGENT

The use of indicator reagents to detect the presence of a target analyte in a test sample is well known in the art. Depending on the type of diagnostic assay employed, the label employed in the indicator reagent is conjugated to a specific binding reagent that will directly, or indirectly, bind to anti-vaccinia antibody. Formation of an indicator reagent between a specific binding reagent and a label may be any of the conventional types including metal complex labels, radioactive labels, enzyme labels, fluorescent labels, radioactive labels, chemiluminescent labels, and the like.

An important consideration in the design of the rapid vaccinia antibody detection device is that the label chosen in the generation of the indicator reagent should give rise to a readily detectable signal, e.g. a strongly-coloured area easily detectable by the eye. Thus, an important preferred embodiment of the invention is the use of "direct labels", attached to one of the specific binding members. Direct labels are well known in the art and highly advantageous for their use in rapid detection systems. Examples of direct labels include, but are not limited to metal sols, non-metal sols, dye sols, latex particles, carbon sol, and liposome contained colored bodies. Some of their advantages are that they can be used to produce a visually detectable signal without the need to add further reagents, are readily visible to the naked eye without the aid of instrumentation, and can be readily used in a diagnostic device since they are stable when stored in the dry state. With respect to the latter, their stability and immediate release on contact with a buffer reagent can be accomplished by the use of soluble glazes.

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Non-metal sols, such as those of selenium, tellurium and sulfur may be produced according to the methods described in U.S. Patent No. 4,954,452 (Yost, et al). Dye sol particles may be produced as described by Gribnau et al., in U.S. Patent No. 4,373,932 and May et al., WO 88/08534, dyed latex as described by May, supra, Snyder, EP-A 0 280 559 and 0 281 327, and dyes encapsulated in liposomes by Campbell et al., U.S. Patent No. 4,703,017. The use of polymerized dye materials in colloidal form for specific binding assays is also described by in U.S. Patent No. 4,166,105 by Hirschreid which relates to labelled specific binding reagents reactive with specific antigens prepared by linking fluorescent dye molecules to analyte specific antibodies through polymers comprising reactive functional groups. Also of interest is U.S. Patent No. 4,313,734 by Leuvering relating to metal sols, the disclosure of which is incorporated herein by reference; Leuvering, et al., "Sol Particle Immunoassay (SPIA)", Abstract, Journal of Immunoassay, 1(1), pp. 77-91 (1980); Leuvering Dissertation (1984), Sol Particle Immunoassay (SPIA): The Use of Antibody Coated Particles as Labelled Antibodies in Various Types of Immunoassay; Uda et al., Anal. Biochem. 218 (1994), 259-264, DE-OS 41 32 133, page 3, lines 16-18, for applications as markers and Tang et al., Nature 356 (1992), 152-154; Eisenbraun et al., DNA and Cell Biology 12 (1993), 791-797. Furthermore it is also known that non-metallic colloidal particles such as carbon particles (van Amerongen, Anabiotic '92 (1993), 193-199) can also be used. Moeremans, et al., EPO Application No. 158,746 discloses the use of colloidal metal particles as labels in sandwich blot overlay assays. At present colloidal gold particles are used most frequently.

Among the direct labels, metallic sols are preferred, more preferably gold sol particles such as those described by Leuvering in U.S. Patent No. 4,313,734. Leuvering discloses the use of metal sol particles as labels for in vitro determination of immunological components in an aqueous test medium. Specifically disclosed are immunoassay test kits for the detection of antigens or antibodies employing one or more labelled components obtained by coupling the component to particles of an aqueous sol dispersion of a metal, metal compound or polymer nuclei coated with a metal or metal compound having a particle size of at least 5 nm.

The metal sol particles to be used in accordance with the present invention may be prepared by methodology which is known. For instance, the preparation of gold sol particles is disclosed in an article by G. Frens, Nature, 241, 20-22 (1973). Additionally, the metal sol particles may be metal or metal compounds or polymer nuclei coated with metals or metal compounds, all as described in the Leuvering patent mentioned above. In this regard, the metal sol particles may be of platinum, gold, silver or copper or any

number of metal compounds which exhibit characteristic colors.

#### 4.2 COLLOIDAL GOLD PARTICLES

5 Colloidal particles which are suitable as labels according to the invention include those which may be conjugated to specific binding reagents without interfering with the activity of such reagents or with other reagents or analytes.

10 Colloidal metal particles are particularly suitable as labels according to the present invention and include those particles which are comprised of metals or metal compounds selected from the group consisting of the metals platinum, gold, silver and copper and the metal compounds, silver iodide, silver bromide, copper hydroxide, iron oxide, iron hydroxide or hydrous oxide, aluminum hydroxide, or hydrous oxide, chromium hydroxide or hydrous hydroxide, lead sulfide, mercury sulphide, barium sulphate and titanium  
15 dioxide. Preferred colloidal metal particles include those made up of gold.

Colloidal gold particle markers are simple to use in comparison to other conventional markers. For example, they do not require instruments necessary for detection of other markers such as radioactive isotopes and unlike enzymes, they do not require the  
20 additional step of adding a substrate.

Colloidal gold particles may be produced according to methods generally known in the art. Of interest to the present invention are those references relating to the use of dispersions of colloidal particles in immunological assay procedures. Specifically, Frens, Nature, 241,  
25 20-23 (1973) discloses methods for the production of gold sol particles of varying sizes through the reduction of gold chloride with aqueous sodium citrate. The colors of the visually detectable signal from the metal particle label is dependent upon the identity and particle size of the metal particle which may be controlled by varying the concentration of the reactants. For example, colloidal gold particles produce colors ranging from orange to  
30 red to violet depending upon the particle size of the sol.

The colloidal gold reagent is selected for its unusual properties: the ability to intensify color to the naked eye when concentrated on solid surfaces, the ability to minimally bind nonspecifically to solid surfaces, the ability to be prepared in relatively uniform particle  
35 sizes, and the ability to be easily lyophilized and resolubilized. Colloidal gold particles can be prepared in a number of ways through the reduction of tetrachloroauric acid which produces a variety of particle sizes ranging from 5 nm to 100 nm. The preferred particle

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sizes are from 15 to 20 nm. The colloidal gold particles can have an intermediary binder absorbed to its surface prior to the addition of the binding substance, but direct attachment is satisfactory. Absorbing the selected binding substance is achieved by carefully controlling concentrations, ionic strength and pH of the reaction mixture. The choice of method of producing the colloidal gold raw material or the method of attaching the binding substance are well known to those skilled in the art. After the labeling with colloidal gold is complete, the reagent is differentially centrifuged or filtered to control particle size. Particle sizing by gel filtration methods are also well known. The colloidal gold labeled reagent can be used as a colloidal suspension or as a lyophilized reagent with or without the presence of the aforesaid solid phase particles as an indicator reagent.

The resulting coated and stabilized colloidal metal particles may then be conjugated with various proteins. Any protein which may be subjected to freeze-drying or other forms of drying such as by incubator, air-drying and spray drying may be applied in the present invention. Exemplary of protein for use in the present invention includes, but is not limited to, polyclonal or monoclonal antibodies, antigen, lectin, protein A, protein G, bacterial, and the like. A preferred methods of detecting the presence of anti- vaccinia antibody is the utilization of a labeled Protein A colloidal gold conjugate.

For details and engineering principles involved in the synthesis of colored particle conjugates see Horisberger, Evaluation of Colloidal Gold as a Cytochromic Marker for Transmission and Scanning Electron Microscopy, Biol. Cellulaire, 36, 253-258 (1979); Leuvering et al, Sol Particle Immunoassay, J. Immunoassay 1 (1), 77-91 (1980), and Frens, Controlled Nucleation for the Regulation of the Particle Size in Monodisperse Gold Suspensions, Nature, Physical Science, 241, pp. 20-22 (1973). Surek, et al., Biochem. and Biophys. Res. Comm., 121, 284-289 (1984) discloses the use of protein A labeled colloidal gold particles for the detection of specific antigens immobilized on nitrocellulose membranes.

#### 4.3 DRYING PROCESS - SUGAR/GLAZING TREATMENT

According to one important aspect of the invention, the indicator reagent is impregnated and dried within the thickness of the porous material defining the label zone of the post-filter unit, which may then be resolubilized by addition of the push buffer. Thus, by incorporating one of the detection test reagents in the device of the present invention, makes possible the reduction in the number of steps required in the detection test protocol by eliminating the addition and/or prior mixing of an indicator reagent.

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In order to assist the free mobility of the indicator reagent when the label zone of the post-filter unit is moistened with the push buffer, the post-filter unit is pre-treated with a glazing material in the region to which the indicator reagent is applied. Glazing can be achieved, for example, by depositing an aqueous sugar or cellulose solution, e.g. of sucrose or lactose, on the relevant region of the post-filter unit, while avoiding the remainder of the filter unit, and air drying. The indicator reagent can then be applied to the glazed portion.

The glazing process involving the use of one or more sugars (e.g. glucose, lactose, trehalose and sucrose) is highly advantageous when employing the dried indicator reagent of the present invention in that the sugar serves (1) as a protein stabilizer, (2) to improve the long term stability of the dried indicator reagent, and (3) acts as a rapid releasing agent. According to a preferred embodiment of the invention, sucrose was determined to be the best sugar compared to others in the performance of the detection test because of (1) its solubility, (2) short period of drying, (3) the overall sensitivity of the detection test result, (4) its use as a preservative, and (5) it is economical to use.

#### 5.0 BUFFER REAGENT

Conventional detection assays usually necessitate the use of two or more fluid reagents in order to perform various steps of the assay protocol including, for example, resolubilizing a dried indicator reagent, diluting a biological test sample, blocking the membrane surface where the assay reaction takes place, facilitating transport of critical reagents and/or washing unbound reactants from the reaction zone. Since each of these steps involves the mixing or preparation of different reactants, different formulations of liquid reagents are likely required due to differing pH, ionic strength, additives, type and strength of buffer, temperature, etc. For example, the resolubilization process usually requires the use of a physiological buffer such as buffered saline or double distilled water, the blocking process uses a liquid reagent formulated with any number of animal serum albumins, gelatin or non-fat milk, and the washing and/or diluting process involves the use of a phosphate buffered saline containing different amounts of surfactant or detergent at neutral pH to remove any non-specific binding reactants. Moreover, in order to ensure that the user performs each step of the assay correctly using the appropriate liquid reagent, the reagents themselves must be clearly labeled and readily distinguished from one another, so as to avoid any possible confusion and user error.

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An important aspect of the present invention overcomes the various problems described above by providing a push buffer which is a multifunctional in that it serves as a single buffer reagent for utilization in the aforementioned 2-step detection test procedure. The push buffer is formulated to serve as a combination resolubilization reagent of the dried indicator reagent, transport facilitating reagent of resolubilized indicator reagent from the label zone of the post-filter unit to reaction zone of the test unit, and washing reagent to remove unbound reactants from the reaction zone. Moreover, since the reaction zone of the present invention is already pretreated with conventional blocking agents following immobilization of the vaccinia viral lysate, the buffer formulation eliminates the need to include a non-specific blocking agent. In order to simplify the number of reagents and steps required to perform the detection test, the push buffer has been specially formulated to be used in conjunction with the dried indicator reagent. It is therefore, particularly advantageous to utilize the push buffer and dried indicator reagent as a combined system since they allow optimal sensitivity and higher specificity to be achieved during performance of the detection test. Additionally, aggregation and inactivation of the indicator reagent in solution is avoided without sacrificing either the sensitivity or specificity of the detection test. A method of using the push buffer as provided by the present invention involves dropwise addition of the buffer to the post-filter unit in a single application of the 2-step detection test to resolubilize the dried indicator reagent. A kit containing the push buffer as a component is also provided.

Accordingly, the present invention provides an improved buffer formulation for use with the rapid vaccinia antibody detection device, comprising a biological buffer (e.g. phosphate buffer) in a sufficient concentration to maintain the pH between 7.0 to 10.0; at least one surfactant (e.g. Triton®X-100); a high molecular weight polymer (e.g. polyvinylpyrrolidone); a pH stabilizer (e.g. trizma hydrochloride); an ionic salt (e.g. NaCl); and a calcium chelator (e.g. EDTA); all at effective concentrations. The buffer also can include sodium azide and thimerosal as preservatives at an effective concentration to reduce bacterial and microbial growth and thus, prolong the shelf life of the reagent.

The push buffer composition of the invention can include a conventional buffer such as a phosphate buffer, MES (morpholino-ethanesulfonic acid) buffers, BIS-TRIS buffers, citrate buffers, TRIS-HCl buffers and borate buffers, at an effective concentration which can range from about 10 to 100 mM, preferably in the range of from about 10 to 30 mM, and most preferably about 20 mM. The preferred buffer is a phosphate buffer, preferably comprising sodium phosphate, monobasic and sodium phosphate, dibasic, at concentrations such that the effective concentration of buffer is achieved. The pH of the buffer of the present



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invention can range from a pH of about 7.0 to a pH of about 10.0.

The biological detergents (surfactants) used in the present invention can include non-ionic surfactants, anionic surfactants, zwitterionic surfactants and cationic surfactants. The  
5 Non-ionic detergents useful in the invention include polyoxyethylene sorbitan monolaurate (Tween®20), polyoxyethylene sorbitan monooleate (Tween®80), polyoxyethylene ethers (Triton®, Brij®) and octylphenol ethylene oxide (Nonidet®). Preferably, non-ionic detergents are used. The most preferred non-ionic detergent is Triton®X-100. Non-ionic detergent acts as a dispersing agent to reduce the non-specific binding of  
10 antibodies/antigens to the reaction membrane which may occur as a result of target analyte adhering to the solid phase due to a non-specific reaction, thereby increasing the background of the assay. Although biological detergents reduce the event of such binding caused by nonpolar or hydrophobic interactions, non-ionic detergents are preferred for their ability to reduce non-specific binding while avoiding the inhibition of specific binding.  
15 Effective concentrations of the biological detergent range from about 0.005 to about 0.06%, (w/v) preferably range from about 0.01 to about 0.025%, and most preferably the concentration is about 0.017%.

Effective concentrations of sodium chloride range from about 0 to about 300 mM,  
20 preferably range from about 100 to about 200 mM, and most preferably the concentration of sodium chloride is about 150 mM.

Polyvinylpyrrolidone functions as a dispersing and suspending agent while additionally preserving the binding capacity of antibodies by blocking non-specific sites on the reaction  
25 membrane. Effective concentrations of polyvinylpyrrolidone (PVP) in the buffer of the invention range from about 0.1 to about 3.0%, (w/v) preferably range from about 0.5 to about 2.5%, and most preferably the concentration is about 1.4%. The high molecular weight polymer selected for use in the invention can include PVP having molecular weights of from about 10 kD to about 1500 kD, dextrans with molecular weights ranging from  
30 about 10 kD to about 2000 kD, polyethylene glycols (PEG) having molecular weights in the range of from about 200 D to about 10,000 D, polyvinyl alcohol having a molecular weight of about 10,000 D to about 100,000 D, polybrene (hexadimethrine bromide), methylcellulose, gum acacia, protamine sulfate, merquat, celquat and magnafloc, provided at an effective concentration. The preferred high molecular weight polymer is PVP; most  
35 preferably, PVP-40 is provided at an effective concentration.

The addition of a calcium chelator, preferably, preferably EDTA, to the push buffer

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composition is essential to prevent the possible clotting of a test sample through calcium-depleting action. The effective concentration of EDTA is from about 10 to 100 mM.

The pH stabilizer functions to maintain the pH of the buffer within a range of about pH 7.0 to 10.0. An exemplary pH stabilizer includes trizma hydrochloride, although other known stabilizers may also be useful in this composition. The effective concentration of trizma hydrochloride is from about 0.02 to 0.05 mM.

## 6.0 HOUSING

In general, the detection test composite comprising the test unit and the post-filter unit can be housed in a suitable container to form a detection apparatus. Preferably, the container should safeguard the solid phase materials and dried indicator reagent from contamination and to provide ease and convenience in handling of the detection test device. Moreover, the container should be leak-proof thereby ensuring containment of fluids and their safe disposal after use.

The apparatus **13** illustrated in Figures 3 and 4 provides a representative example of the type of container that can be included in a test kit which incorporates the flow-through detection test of the present invention. The apparatus **13** comprises two detachable components, namely the test cartridge **14** and the post-filter cap **15**, which are vertically and spacially distinct to one another when placed in transient communication during the detection test protocol. The housing is capable of maintaining the layers of the test unit under compression so as to provide continuous and uniform contact therebetween and so that liquid will flow uniformly through the apparatus **13**. The housing will be made of an inert material conveniently being any of a variety of disposable commercial plastics which may be molded, for example, polyethylene, polypropylene, styrene, ABS, polyacrylate, polystyrene, or the like.

Although the two components of the apparatus **13** have the particular configuration and dimensions depicted therein, any other appropriate design or modifications may be employed so long as the components are still capable of being transiently connected to one another in a single movement during the detection test protocol. The means of connecting the two components is not critical so long as so that they are properly aligned to effect optimal fluid communication with one another upon interconnection of the post-filter cap **15** with the test cartridge **14**. For example, according to the design shown in Figures 3 and 4, the post-filter cap **15** may be frictionally fitted to the reservoir **22** of the test

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cartridge **14**. Although not illustrated therein, the post-filter cap **15** may be optionally hinged to the test cartridge **14** to avoid possible lost or misplacement of the two components. On the other hand, the two components could be slidably and reversibly disposed to one another in a single horizontal movement providing the post-filter unit is engaged in proper alignment above the test unit. In this particular instance, proper alignment of the two components may be achieved through the use of guide rails, or projections designed to align with recesses formed in the device or housing, additionally acting as an interconnection means for the two components.

The precise dimensions of the housing are not essential to the function of the detection test apparatus, but in general, the apparatus will be of a size convenient for transport, manipulation, and assembly. The housing will generally have a length in the range of about 2 to 5 cm, preferably 3.5 cm. The width will be in the range of about 1 to 3 cm, preferably 2.5 cm. The height of the housing will be in the range of about 0.5 to 5 cm, preferably 1.3 cm.

Figure 3 provides an exploded view of the apparatus **13** comprising the test unit **2** and the post-filter unit **3**, while Figure 4 provides an enlarged vertical cross-sectional view of the fully assembled apparatus **13**. The apparatus **13** of the present invention comprises two separate components in its fully assembled form, namely the test cartridge **14**, which contains the test unit **2**, and the post-filter cap **15**, which contains the post-filter unit **3**. The test cartridge **14** and the post-filter cap **15** are designed to be connected to one another briefly during the detection test protocol. The apparatus **13** is intended to be simple in design and construction, and can be manufactured using readily available materials.

As shown in Figure 3, the test cartridge **14** of the apparatus **13** houses the test unit **2** which comprises both a top member **16** and a bottom member **17**. The outer perimeter of the bottom member **17** has a slightly indented ridge **18** which allows it to be fitted and interconnected with the rim **19** bordering the top member **16** to form the assembled test cartridge **14**. It will be appreciated by those skilled in the art that while the test cartridge **14** shown in Figures 3 and 4 has a rectangular shape, it is not limited to this particular configuration so long as it can be adapted to hold the absorbent material, or pad **20**, in direct contact with the porous reaction membrane **21**.

Contained within the top member **16** of the test cartridge **14** is a reservoir **22** which is in direct alignment with the exposed reaction membrane **21** of the test unit **2**. The reservoir

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**22** (a) provides access to the reaction zone **5** for introducing the fluid sample, (b) provides operable attachment of the post-filter cap **15** for introduction of the push buffer, and (c) permits viewing of the "indicator" zone(s) on the reaction membrane **21** following removal of the post-filter cap **15**, i.e. detect the color, or fluorescence, or other signal, in the indicator zone(s). As depicted in the drawing, the upper surface surrounding the reservoir **22** is slightly curved and extended downwards so as to form a cup-like receptacle which terminates at, and firmly engages a portion of the reaction membrane **21**. In this way, the amount of test sample introduced into the reservoir **22** cannot bypass any components of the apparatus **13**. The configuration of the inner wall **23** and the dimensions of the reservoir **22** are selected so that the reservoir **22** can connect to and be in operable association with the post-filter cap **15** during the detection test protocol. Preferably, both the reservoir **22** and the post-filter cap **15** have a funnel shape configuration. Thus, when the reservoir **22** and the post-filter cap **15** are in the operating position and the push buffer is applied to the filter cap **15**, this configuration will permit a large amount of the buffer to contact and pass through a small amount of surface area of the reaction membrane **21**. Thus, by selectively matching the size of reservoir **22** with the post-filter cap **15**, the operation of the apparatus **13** can be simplified so that, for example, the push buffer **12** can be delivered to the reservoir **22** in a single step of the detection test procedure.

According to the embodiment shown in Figures 3 and 4, the post-filter cap **15** is detachable affixed to the reservoir **22** of the test cartridge **14** by means of a friction fit between the inner wall **23** of the reservoir **22** and the external wall **33'** of the filter cap **15**. Such other means for detachable affixing the post-filter cap **15** to the test cartridge **14** can be used. In addition, the height of the external wall **33'** of the post-filter cap **15** is slightly less than the height of the inner wall **23** of the reservoir **22** so that when the filter cap **15** is affixed to the reservoir **22**, the base **24** of the filter cap **15** terminates immediately above, but not touching, the reaction membrane **21**. The dimensions of both the reservoir **22** and the post-filter cap **15** can be varied considerably without affecting the performance of the apparatus **13**, although the following approximate dimensions have been determined as satisfactory: reservoir **22** - 1.5 cm top and bottom diameters and 0.6 cm deep; post-filter cap **15** - 0.9 cm bottom diameter, 1.1 cm top diameter, and 0.5 cm deep.

As described above, the test unit **2** of the present invention comprises a porous reaction membrane **21** and an absorbent pad **20**, whereby the lower surface of the reaction membrane **21** is supported by the upper surface of the absorbent pad **20**. The reaction membrane **21**, which contains vaccinia viral lysate as capture reagent, essentially defines

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the reaction zone in which various specific binding reactions take place during the detection test. As previously described, the reaction membrane **21** can be fabricated from a number of biologically inert, porous materials.

5 Positioned directly underneath the lower surface of the reaction membrane **21**, and in fluid communication therewith, is an absorbent pad **20** defining the absorbent zone. In embodiments of the invention where ease of manufacture and reduced costs are desired, the entire upper surface of the absorbent pad **20** is typically immediately adjacent the lower surface of the reaction membrane **21**. The test unit **2** may optionally include a  
10 separating means between the reaction membrane **21** and the absorbent pad **20** which will generally be incapable of binding the anti-vaccinia virus antibodies. According to the embodiment shown in Figure 3, the separating means in the form of a spacer layer **25** substantially isolates the reaction membrane **21** from the absorbent pad **20**. Although not critical to the performance of the apparatus **13**, the spacer layer **25** serves to hold the  
15 porous reaction membrane **21** and permit test reagents to flow uniformly from the upper surface down to the lower surface of the detection test apparatus **13**. The spacer layer **25** may be made of any rigid or semi-rigid porous material that does not bind or interact with test reagents used in conjunction with the invention. Exemplary of materials for the spacer layer **25** are fiberglass, paper, hydrophilic polypropylene, and cellulose; preferably the  
20 spacer layer **25** is made of H-HDC (Pall). The thickness of the spacer layer **26** will generally be in the range of about 0.1 mm to 1 mm.

The spacer layer **25** has an aperture **26** defined by a rim **27** which has similar circumferential dimensions and/or shape as the porous reaction membrane **21** thereby  
25 enabling the upper and lower surfaces of the reaction membrane **21** to be accessible when the membrane **21** and the spacer layer **25** are sealed together to form a press-fit piece. Referring to Figure 3, which depicts one embodiment of the apparatus **13**, a portion of the reaction membrane's **21** upper surface is fully exposed so that when the detection test is performed, the fluid test sample and the test reagents can be added directly to the reaction  
30 membrane **21**. The reaction membrane **21** is sized to completely cover the aperture **26**. Preferably the reaction membrane **21** will be the same shape as the aperture **26** and but sized slightly larger than the aperture **26** so that it can be sealed to the lower surface of the spacer layer **25** at the periphery of the aperture **26**. However, the shape of the reaction membrane **21** and the shape of the aperture **26** can differ and are not limited to  
35 the configuration shown in Figure 3. Thus, in combination, the rim **27** surrounding the aperture **26** and the exposed upper surface of the reaction membrane **21** define a test zone. Moreover, after the test cartridge **14** of the apparatus **13** is assembled, the

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absorbent pad **20** is still capable of contacting the lower surface of reaction membrane **21** located directly beneath the reaction membrane **21**. The dimensions of the spacer layer **25** and the absorbent pad **20** are chosen to fit cooperatively within the base of the test cartridge **14**, thereby ensuring that the absorbent pad **20** is in proper alignment and fluid communication with the lower surface of reaction membrane **21**. Thus, the surface area of the upper surface of the absorbent pad **20** will usually be greater than that of the reaction membrane **21**, but similar to that of the spacer layer **25**.

The absorbent pad **20** is selected to have a capillary pore size so as to induce flow of the fluid test sample through the reaction membrane **21** without the use of external means. Thus, conveniently, the absorbent pad **20** serves to both promote and direct the flow of reagents through the porous reaction membrane **21**. The absorbent pad **20** is of sufficient size and composition so that it is capable of absorbing excess sample, indicator reagent and buffer. The material from which the absorbent pad **20** is fabricated may be any non-porous wettable material that is substantially inert to the test reagents employed in the performance of an detection test. The absorbent pad **20** will be of essentially the same dimensions and shape as the spacer layer **25** which holds the porous reaction membrane **21**. The precise thickness of the absorbent pad **20** is not essential to the function of the present invention, generally ranging from about 2 to 10 mm.

The second component of the apparatus is the funnel-shaped post-filter cap **15** which readily accommodates a sufficient amount of the push buffer needed to perform the detection test in a single application. The post-filter cap **15** comprises the post-filter unit **3** and inner **28** and outer **29** sleeves being open-ended at both the top and bottom. The bottom opening **30,30'** of sleeves **28** and **29** is sized to achieve the flow rate desired for the detection test in question. The opening of the sleeves can conveniently have a diameter in the range of 12.6 to 15.2 mm. Preferably the opening **30,30'** diameter is 9.5 mm.

In the assembled form, the post-filter cap **15** comprises a funnel **31** having at its top outwardly extending flanges **32, 32'** and depending sidewalls **33,33'**. The depending sidewalls **33** of the outer sleeve **29** end at a base **24**. The opening **30** in the base **24** allows a stream of fluid traveling through the funnel **31** to flow into the test cartridge **14**. The post-filter unit **3** of the present invention is securely held in the base **24** of post-filter cap **15** by the inner **28** and outer sleeves **29** of the post-filter cap **15**. An inner collar **34**, integrally formed at the base **24** of the outer sleeve **29**, is capable of supporting the post-

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filter unit **3** so that when the inner sleeve **28** is frictionally fitted inside the outer sleeve **29**, the post-filter unit **3** will be held permanently in place.

The post-filter unit **3** comprises a filter medium impregnated with dried indicator reagent which defines the label zone. The dried indicator reagent is resolubilized and transported by the push buffer to the reaction membrane **21** following addition of the buffer to the post-filter cap **15**. The selection of the filter medium for the post-filter unit **3** is not critical to the invention and can be any suitably absorbent, porous or capillary possessing material through which the push buffer and resolubilized indicator reagent may be transported by wicking action. The criteria of selection is that the material allow for the resolubilization and mixing of the dried indicator reagent upon addition of the push buffer, as well as initiate the transfer of the buffer and freshly dissolved indicator reagent to the reaction membrane **21** of the test unit **2**.

For convenience of manipulation in using the apparatus **13**, a handle **35** is secured to the extending flanges **32,32'** of post-filter cap **15** so that when the filter cap **15** is affixed to the reservoir **22**, it extends slightly beyond the boundary of the reservoir **22** for ease of removal of the post-filter cap **15** from the test cartridge **14**.

A representative example of a modified version of the test cartridge of the invention incorporating a blood separation zone contiguous with the reaction zone for the detection of analyte in a whole blood sample is illustrated in Figures 6A and 6B.

As shown in Figure 6A, the test cartridge is provided with a top member **16** constructed and adapted to fit snugly with a bottom member **17**. In this particular embodiment, the top member **16** of the test cartridge defines a first opening or internal recess therethrough in the form of a reservoir **22**. The reservoir **22** serves to (a) provide operable attachment of the post-filter cap for introduction of the push buffer, and (b) permit viewing of the "indicator" zone(s) on the membrane following removal of the post-filter cap, i.e. detect the color or fluorescence, or other signal, in the indicator zone(s). Thus, the configuration and dimensions of the reservoir **22** are selected on the basis that it can be operably connected to the post-filter cap to enable transient fluid communication between the label zone of the post-filter unit and the reaction zone of the test unit.

Spaced a short lateral distance from the reservoir **22**, the top member defines a second opening therethrough in the form of a reservoir **104** which may, as shown, have beveled sides, or may be in any shape or size or configuration of convenience which will sufficiently

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direct and provide access to the first end of the blood separation zone upon application of a whole blood sample. After introducing a whole blood sample to the reservoir **104** and allowing for a short incubation time to enable sufficient separation and migration of the RBC-free fluid along the blood separation zone to the reaction zone, the post-filter cap is operably attached to the reservoir **22** to enable completion of the 2-step detection test protocol so that a final determination for the presence of analyte can be made.

As shown in Figure 6B, the bottom member **17** of the test cartridge provides a first base structure **105** having a plurality of supporting walls which serve as a solid enclosure for the absorbent pad and thus, is configured to receive and hold the absorbent pad securely in place. Additionally provided is a second base structure **106** having a plurality of protruding columns of the same height which serves as an elevated support for the blood separation zone. The position of the second base structure **106** in relation to the first base structure **105**, as well as its configuration, are such that when the blood separation zone is positioned within the bottom member **17**, the blood separation zone is contiguous with and in direct planar horizontal alignment with the reaction zone. Although the base structure **106** depicted therein has a plurality of supporting columns and/or walls which serve to support the perimeter and centre of the blood separation zone, any number of configurations or strategies are possible as long as the blood separation zone is securely and correctly positioned in relation to the reaction zone when the test cartridge is fully assembled.

## 7.0 TEST KIT

The rapid vaccinia antibody detection device of the present invention, which incorporates the test unit and post-filter unit, will typically be packaged in the form of a test kit. The kit will normally include the flow-through detection test device, preferably housed in a suitable container, the push buffer, a disposable plastic pipette and instructions for carrying out the detection test. Such instructions will generally describe the method for carrying out the detection test protocol including the relative amounts of test sample and push buffer to be added to the test unit and post-filter unit, respectively.

Preferably, the detection device is housed within a suitable container which comprises two detachable components, each component separately containing the test unit and the post-filter unit, which are arranged in a vertically and spatially distinct format. In particular, the design of the container should allow the test unit and post-filter unit to be operably connected to one another so that the reaction zone and the label zone can be placed in



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transient fluid communication with one another during the detection test protocol. The container housing the test unit should be capable of maintaining the layers of the test unit under compression so as to provide continuous and uniform contact therebetween so that liquid will flow uniformly through the apparatus. Figures 3, 4 and 6 provide a representative example of the type of container that can be included in a test kit which incorporates the flow-through format of the rapid vaccinia antibody detection device.

All publications and patent applications mentioned in this specification are indicative of the level of skill of those skilled in the art to which this invention pertains. All publications and patent applications are herein incorporated by reference to the same extent as if each individual publication or patent application was specifically and individually indicated to be incorporated by reference.

The invention will be further understood from the following non-limiting examples. The following examples are provided to describe in detail some of the representative, presently preferred methods and materials of the invention. These examples are provided for purposes of illustration of the inventive concepts, and are not intended to limit the scope of the invention as defined by the appended claims.

## 8.0 EXAMPLES

The foregoing is a general description of the apparatus, method and reagents of the invention for the detection of anti-vaccinia virus antibody. Although dye sols, gold sols or coloured latex particles may be linked to Protein A to form the indicator reagent, the preferred visual label utilized in the example detection test will be colloidal gold particles. Using an apparatus comprising the test unit and post-filter unit, such as the one illustrated in Figures 3 and 4, and by performing the 2-step rapid detection test of the present invention, a determination of antibody against vaccinia virus in a whole blood or serum test sample can be made in less than three minutes.

### 8.1 VACCINATION COMPLICATIONS

Certain groups of people are at high risk for complications if such a mass vaccination program were to be implemented. Immunodeficient individuals, such as HIV/AIDS patients, would be prone to Progressive Vaccinia (or vaccinia necrosum), a dermal complication resulting from exposure of immunocompromised individuals to the vaccinia virus (WHO, 2001). Specifically Progressive Vaccinia could prove to be deadly to an HIV-

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infected individual resulting from an accidental or inadvertent vaccination with the vaccinia virus or through direct contact with a person who had been recently vaccinated (Shanley, 2002). For example, vaccination of an HIV/AIDS patient with the vaccinia virus could result in death within a few months following. Mortality rates associated with this condition were  
5 nearly 100% in the 1950's and early 60's but drastically decreased to 33% with the advent of vaccinia immune globulin (VIG) in 1969 (Kaufman, 2001). Such individuals will develop secondary lesions, which will progressively spread until death. As a result, knowing an individual's HIV status prior to small pox vaccination must be a mandatory requirement. The commercially available MedMira Reveal™ HIV test will provide an efficient means to  
10 ensure that HIV testing can be provided immediately prior to vaccination whereas conventional laboratory testing for HIV can take days for results. Thus, it is recommended that the MedMira Reveal™ Rapid HIV test should be used in conjunction with the smallpox vaccination program to eliminate the complications associated with vaccination.

15 The 114 million young Americans who have not been vaccinated against smallpox also fall into the high-risk group for HIV-infection (Henderson et al., 1999). The entire United States population of almost 300 million (2001) will require prevaccination screening for rapid diagnosis of HIV to aid in avoidance of the potential tragedy of "preventable death" due to the wrongful administration of the smallpox vaccine to immune-deficient individuals.  
20 In following the lead of the Americans, who are considered by many countries worldwide to maintain the highest of public health standards, other developed nations encompassing a population of approximately 1.2 billion (2001) may also implement this testing/vaccination algorithm.

## 25 8.2 PREPARATION OF VACCINIA VIRUS CELL LYSATE

The seed virus (V-CL) used in this particular preparation was obtained from Connaught Medical Research Laboratories in Toronto, Ontario. It is a standard strain of vaccinia virus produced through routine preparation of calf lymph.

30 Vaccinia virus preparation involves the infection of a monolayer of HeLa cells with a  $10^{-2}$  dilution of frozen virus stock. The culture is then incubated for 2 to 3 days at 36°C. Once destruction of the HeLa cells is complete, the culture was subjected to a freeze/thaw cycle three times and then disrupted for 15 minutes in the cooled water bath of an ultrasonic  
35 vibrator. Cell debris is removed by low speed centrifugation (2,000 rpm for 20 minutes) and the resulting supernatant fluid is collected and stored at -20°C in 1 mL volumes until used.

### 8.3 RAPID FLOW-THROUGH MEMBRANE APPLICATION

The resulting supernatant containing the soluble viral lysates was diluted to 1:8 in carbonate buffer (pH 9.0) containing 0.5% sucrose and 5 mM NaCl. This preparation was then subjected to a 0.45  $\mu$ m filtration process and the resulting clear fluid was used as the final cocktail for immunobinding application on a paper-backed nitrocellulose membrane using a DioDot printing device. The cocktail was imprinted on the cellulose paper in a horizontal line format.

### 8.4 PREPARATION OF THE DETECTION TEST APPARATUS

The apparatus **13**, illustrated in Figures 4 and 5 and comprising a test cartridge **14** and post-filter cap **15**, represents a suitable container to house the test unit **29** and post-filter unit **30** of the present invention.

#### I. Test Cartridge

The test cartridge, which houses the test unit of the rapid test device, is made of clean technical grade white polypropylene plastic and has a top **16** and bottom **17** component. Both are made in synchronized 16 cavity mold, precisely engineered to allow a snugly fitting tight seal when the two components are pressed together. The components are supplied as individual casings by Top View International Limited, Hong Kong, and are assembled at the manufacturing plant of MedMira Laboratories, Halifax, Canada. These components meet the following criteria:

- Appearance - a clear, white smooth texture of the plastic.
- A snug fit to produce a leak-proof housing to ensure safe containment of all applied liquids.
- Consistency of dimensions to specifications of 2.5 cm width, 3.5 cm length, and 1.3 cm height.
- Consistency of dimensions of the reservoir **22** opening of 1.6 cm in diameter and a formed cylinder depth of 0.5 cm.
- Consistency in the location of the reservoir **22** in the top component of the test cartridge **14**.

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#### A. Reaction Membrane

A porous reaction membrane **21** such as nitrocellulose having an average pore size of 0.45 microns (Whatman, England) is used and cut to 12 mm x 12 mm. The membrane **21** is 0.2 mm paper-backed and specially treated for enhanced protein binding. Certified specifications given by the manufacturer (Whatman, England) include a binding capacity of 80-90 mg protein/cm<sup>2</sup>, a water flow rate of 6 ml/min/cm<sup>2</sup> and a bubble point of 3.5 bar. The reaction membrane **21** is prepared having two immunoreactive test sites, namely a test zone and a control zone, each zone produced in the shape of a distinct vertical line. The control line and the test line are positioned perpendicular to, but not touching, one another to provide a clear differentiation between the two. The test zone of the membrane is prepared by applying a solution of vaccinia viral lysate in carbonate buffer (pH 9) using a printer device (BioJet Quanti 3000 dispenser). The control zone is similarly prepared by applying a mixture of a specially calibrated antigen preparation that binds to all classes of IgG antibodies ordinarily present in a biological fluid sample regardless of HIV IgG antibody status, and thus serves as a control zone. After the membrane is dried at room temperature for 10 minutes, it is treated with a solution of 1% bovine serum albumin in 0.1 M sodium phosphate buffer and allowed to completely dry at ambient temperature for approximately 24 hours.

#### B. Optional Spacer Layer

A spacer layer **26** supporting the reaction membrane **21** may be produced by securing the outer perimeter of the upper surface of the porous reaction membrane **21** to the lower surface of the porous spacer layer **26** such that the upper surface of the reaction membrane **21** is exposed through the aperture of the spacer layer **26**. The upper surface of the reaction membrane **21** is sealed to the lower surface of the spacer layer with a water-insoluble adhesive so as to form an impermeable seal between the rim **28** of the spacer layer **26**, defining the aperture **27**, and the unexposed upper surface of the reaction membrane **21**. This arrangement helps to promote the flow of fluids in a downward, as opposed to lateral, direction through the reaction membrane **21** and into the absorbent pad **20** below. The spacer layer **26** may be purchased with water-soluble adhesive already adhered to the lower surface, or the adhesive may be applied during the manufacturing process. The spacer layer is a polystyrene material insert with a double-sided tape (Halifax Folding Company, Nova Scotia, Canada). The reaction membrane **21** is secured to the spacer layer **26** by the double-sided tape. The assembled spacer layer **26** is approximately 29.0mm x 20.5mm in area and 1.0 mm in thickness and is positioned on the upper surface

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of the absorbent pad **20** which sits in the base of the test cartridge **14** as shown in Figures 4 and 5.

### C. Absorbent Pad

5 The absorbent pad **20** is placed directly beneath the reaction membrane **21** and securely inside the bottom member of the test cartridge **14**. The pad **20** is composed of thickened compressed cellulose acetate with a porosity of 40 ml/min (Filtrona, Richmond Inc., Richmond, VA). It is made of synthetic fibers without the use of resins or adhesives and provides an excellent level of aqueous fluid compatibility. Void space is specified at 80 to  
10 85% and absorption of liquids at 6 times the dry unit weight and up to 90% of the total void volume. It is resistant to pH in the range of 2.5 to 9.5. The pad **20** is die cut to a specification of 2.2 cm width, 3.2 cm length and 0.5 cm height. The pad **20** fits securely into the bottom component **17** of the test cartridge **14** so as to create a compressed composite of the reaction membrane **21** with the absorbent pad **20** to ensure a continuum  
15 of fluid communication between the porous materials for enhanced hydrodynamics and complete absorption when test samples are applied to the reaction membrane **21**.

### II. Post-Filter Cap

The post-filter cap **15**, which houses the post-filter unit **30** of the rapid test apparatus **13**,  
20 is comprised of an outer funnel sleeve **32** having an internal collar **37** at its base, an inner funnel sleeve **31** having a handle **38** extending therefrom, and the post-filter unit **30**. The funnel sleeves **31,32** and the handle **38** are molded from a plastic material. One preferred plastic material is polystyrene resin (Fouzhou Chimoplus Chemical Company Ltd., China). The outer **32** and inner **31** funnel sleeves are cylindrical in shape with an outside diameter  
25 of 15.0 mm and 12.5 mm, respectively and the assembled cap **15** fits snugly into the reservoir **22** of the test cartridge **14**. The post-filter cap **15** is designed to be connected to the reservoir **22** of the test cartridge **14** following post-application of the test sample to the reservoir **22**, and removed shortly after the push buffer has been added and diffused through the post-filter unit **30** of the filter cap **15**. In the assembled form, the volume  
30 capacity of the post-filter cap **15** is 0.5 ml.

The post-filter unit **30** is comprised of one filter layer that will be in direct contact with the reaction membrane to improve the subsequent reactivity between the antibodies of the colloidal gold conjugate and the antigen-coated reaction membrane. The filter is comprised  
35 of glass micro fiber with OVA binder (Whatman, GF/AVA) which is white and has a basis weight of 48 g/m<sup>2</sup>, a thickness of 303 mm, a flow rate of 150 s/1.5 cm, dry tensile of 640 g/1.5 cm, wet tensile of 324 g/1.5 cm and a porosity of 3 sec/100 ml/in<sup>2</sup>. Once

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assembled, the freeze-dried colloidal gold conjugate is reconstituted with a solution comprising 0.1-0.15 ml of PBS buffer (0.6-0.7mM potassium chloride, 0.03M sodium chloride, 2-2.1mM di-sodium hydrogen orthophosphate anhydrous, 0.3-0.4 mM potassium phosphate mono) containing 10% sugar. The colloidal gold conjugate solution is dispensed (0.1 to 0.15 ml) onto each filter and then dried at a temperature of 37 to 40°C. The filter layer is die cut according to the following specifications: thickness, 790 to 830 microns; porosity, 1.6 to 2.0 s/100ml/in<sup>2</sup>; tensile strength 14.5N/55mm; flow rate, 67 s/7.5cm; absorbancy, 76.4%; pore size, 4.3 microns; wicking, 1.00 min:sec; and diameter, 0.42 mm.

### 8.5 INSPECTION ON PROTEIN A (PA)

#### Formulation

Sodium Chloride

10% in DDI water

#### BSA

1% BSA in DDI water pH 5.00 to 9.00 (optimum 6.00).

#### Colloidal gold

Prepared up to the pH step.

#### Stock-solution of the Labeling Material

Original concentration diluted in DDI to a final concentration of 0.1 – 2 mg/ml (optimum 0.1mg/ml)

#### Procedure

- Prepare a 9 serial dilution Protein A (PA).
- To the PA, dilution add the colloidal gold already pH adjusted in a 1:10 ratio (e.g. to 0.1 ml of PA dilution add 1ml of colloidal gold).
- Incubate for 10 minutes.
- To each dilution tubes add 8-10 % of sodium chloride to a final concentration of 1% (optimum 0.9%).
- Incubate for 5 minutes.
- To each tube again add 0.07 – 0.1% of bovine serum albumin to a final concentration of 0.1% (optimum 0.08%).
- Read the absorbance at 520 nm.
- The correct concentration of protein is the minimal amount that will inhibit flocculation.

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Conc. ( $\mu$ g)	Absorbance 1	Absorbance 2	Average
0	0,313	0,314	0,314
2	0,524	0,524	0,524
3	0,533	0,532	0,533
4	0,533	0,533	0,533
5	0,540	0,540	0,540
6	0,575	0,571	0,573
7	0,580	0,580	0,580
8	0,576	0,583	0,580
9	0,576	0,576	576

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Hughes D.A & J. E. Beesley (1998) Preparation of Colloidal Gold Probes in (ed) J.D. Pound. *Methods in Molecular Biology vol 80: Immunochemical Protocols, 2<sup>nd</sup> edition*. Humana Press Inc., Totowa, NJ.

## 5 8.6 PREPARATION OF COLLOIDAL GOLD CONJUGATE

### Materials

	Sodium Citrate	0.3 mM in DDI water
	BSA	1% BSA in DDI water, pH 5.00 to 9.00
10	PEG	1% polyethylene glycol (MW 15,000 to 20,000) in DDI water, pH to 6.00
	Phosphate Buffer	mix 0.04M (in DI water) of $\text{NaH}_2\text{PO}_4$ into 0.07M (in water) $\text{KH}_2\text{PO}_4$ in a 1:4.4 ratio; pH to 6.00
	Protein A and	
15	Hepes Buffer	Protein A and Hepes buffer (0.025M Hepes and 0.25mM Thimerosal pH 7.00 in DDI water) in a 1:1 ratio
	Borate buffer	0.05M of sodium borate in DDI water pH 8.50

### Resuspending Buffer

20	8mM di-sodium hydrogen orthophosphate anhydrous
	1% bovine serum albumin
	3mM sodium azide
	0.02% polyethylene glycol
	0.14 - 0.16M sodium chloride
25	1.5mM potassium dihydrogen orthophosphate
	2.7mM potassium chloride
	4.3mM tri-sodium orthophosphate

Mix the above ingredients in 1000 ml of DDI water, pH 7.30 to 7.50.

30

### Procedure

- Add 1% of tetrachloroauric acid to water for a final concentration of 0.01%.
- Let solution reach a hard boiling point.
- Add 15 ml of 0.3mM sodium citrate on a reflux for 30 minutes.
- 35 - Remove the flask and allow the contents to cool to around 40°C or lower.
- Add 60ml of phosphate buffer (mix 0.04M (in DI water) of  $\text{NaH}_2\text{PO}_4$  into 0.07M (in water)  $\text{KH}_2\text{PO}_4$  in a 1:4.4 ratio; pH to 6.00) or 50mM of borate buffer (pH 8.50);



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adjust pH of the colloidal gold to 6.00 – 9.00 (optimal is 6.00), if the pH is too low, add drops of 2mM  $K_2CO_3$ .

- A portion of the solution is removed to perform an aggregation test to know the concentration of the ligand to add to the gold solution.

- 5     - Add Protein A with a final concentration of 5-9 ug/ml + 5% (optimum 6 + 0.3 = 6.3 ug/ml)

$$\frac{[\text{Final PA} + 5\%] \text{ (mg/L)} \times \text{total volume in flask(L)}}{[\text{Initial PA}] \text{ (mg/ml)}}$$

10

i.e. Total volume = 500ml CG and dH<sub>2</sub>O + 15ml sodium citrate + 60ml phosphate buffer – 3ml test for pH = 572ml = 0.572L

$$\frac{(6 + 0.3)\text{mg/l} \times 0.572\text{L}}{1\text{mg/ml}} = 3.60\text{ml Protein A to be added}$$

15

- The solution is allowed to proceed for 15-30 minutes (optimum 20 minutes).
- The absorption of the ligand is stop by adding 10% bovine serum albumin pH 5.00 to 9.00 final concentration of 0.1% stir for 5-15 minutes (optimum 10 minutes).
- 20     - The labeled colloidal gold was centrifuged at a speed of 46,500g (20,000rpm) at a temperature of 4-5°C for 50 to 80 minutes.

#### Aspiration and Re-suspension

- 25     Aspirate the supernatant with the help of a vacuum flask, taking care not to disturb the pellet. Resuspend in re-suspending buffer (or PBS-BSA) to a final optical density of 1.180 to 4.500 (optimum 2.000) at 520 nm.

#### Freeze-dry

- 30     After the appropriate optical density reach, the solution was filled in 0.6 ml aliquots into a 3 ml glass vials. Some rubber freeze-dry stoppers (1-mm in diameter) were inserted halfway into the vials and transferred into the freeze-dryer shelves. A temperature of -40°C was maintained for about 5 hours. The primary drying was carried out at a vacuum of less than 100 mTorr with a shelf temperature of -30°C for about 3 hours and a condenser temperature of less than -80°C. Followed is a shelf temperature of -10°C for
- 35     about 5 hours then a shelf temperature of 0°C, vacuum of 0 mTorr for about 2 hours. A secondary drying is carry on at +20°C for about 4 hours. At the end of the process, the vials were seal under vacuum with the rubber stoppers. The product was then removed

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from the shelves and a functional test was performed to assure the quality of the product. Samples were kept for later reference.

## 8.7 STABILIZATION OF COLLOIDAL GOLD CONJUGATE

### Procedure

- Prepare 1%, 2%, 5% and 10% sucrose in PBS solution, pH 7.0-7.5.
- Reconstitute freeze-dried colloidal gold conjugate with a) 5 drops ( $\sim 150 \mu\text{l}$ ) b) 10 drops ( $\sim 350 \mu\text{l}$ ) and c) 15 drops ( $\sim 650 \mu\text{l}$ ) with each percentage of sucrose.
- Apply 5 drops ( $\sim 150 \mu\text{l}$ ) of each reconstitution to the filter medium.
- Let it air dry completely.

Specimen	Result			
	1%	2%	5%	10%
Control line	2+	2+	2+	3+
Positive control	1+	1+	1+	2+/3+
Negative control	neg	neg	neg	neg

## 8.8 PREPARATION OF THE POST-FILTER UNIT

One of the goals in diagnostic testing is to develop a test device that requires few manipulative steps. Therefore, by associating the indicator reagent with the filter medium of the post-filter unit **30**, it is possible to eliminate extra steps in which the reagents are added separately to the diagnostic device during the detection test protocol.

### Materials

- Colloidal gold conjugate, Prepared and previously freeze-dried as described above.
- Sugar, e.g. trehalose, lactose, sucrose, glucose, maltose, mannose, fructose, etc.

### Procedure

- Reconstitute the freeze-dried colloidal gold with 0.1 – 0.15 ml of PBS buffer (0.6 – 0.7mM potassium chloride, 0.03M Sodium chloride, 2 – 2.1mM di-sodium hydrogen orthophosphate anhydrous, 0.3 – 0.4 mM potassium phosphate mono) containing 10% sucrose.

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- Dispense 0.1 to 0.15 ml of colloidal gold solution onto each filter.
- Let the filter dry completely at 37 - 40°C.

### 8.9 PREPARATION OF THE PUSH BUFFER

5

#### Formulation

0.01 - 0.1M EDTA

0.02M Sodium azide

0.05 - 0.1M Sodium chloride

10 6mM di-sodium hydrogen orthophosphate anhydrous

0.1- 0.25mM Thimerosal

0.05 - 0.1% Triton®X-100

0.02 - 0.03M Trizma hydrochloride

0.2 - 0.3% Tween-20

15 0.5 - 2.5% PVP-40

#### Procedure

- Add all ingredients together (0.01 - 0.1M EDTA, 0.02M sodium azide, 0.05 - 0.1M sodium chloride, 6mM di-sodium hydrogen orthophosphate anhydrous, 0.1- 0.25mM Thimerosal, 0.05 - 0.1% Triton®X-100, 0.02 - 0.03M Trizma hydrochloride, 0.2 - 0.3% Tween-20, 0.5 - 2.5% PVP-40).
- Fill up with DDI water.
- Adjust the pH to 7.00 to 10.00.

20

### 8.10 DETECTION TEST PROTOCOL

25

Using a clean pipette, 1 drop of a serum or plasma sample was added to the centre of the reaction membrane and the sample allowed to absorb completely through the membrane and into the absorbent material pad. The post-filter cap was connected to the reservoir of the test cartridge so that the post-filter unit was in fluid communication with the test unit. Ten to fifteen drops of the push buffer were subsequently added to the funnel of the post-filter cap. After a brief incubation, about 1 minute, during which time the resolubilized colloidal gold conjugate was drawn through the post filter unit, the post-filter cap was removed from the test cartridge. A distinct colored line(s), one vertical control line and one test line, developed in the centre of the reaction membrane indicating the presence of anti-vaccinia virus antibody in the test sample. The results of the detection test were revealed in about three (3) minutes.

30

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**INDUSTRIAL APPLICABILITY**

The rapid vaccinia virus antibody detection device and method taught herein generally provide an improved diagnostic means for the detection of anti-vaccinia virus antibodies in a serum, plasma or whole blood sample, and therefore provide an efficient means for evaluating the efficiency of vaccination, or the need for re-vaccination against smallpox.

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**What is claimed is:**

1. A device (13) for determining the presence or absence of anti-vaccinia virus antibodies (10) in a fluid test sample (9), characterized by:
  - a test unit (2) comprising a reaction zone (5) in vertical communication with an absorbent zone (4), wherein the reaction zone(5) contains a vaccinia viral lysate (6) immobilized therein, said vaccinia viral lysate (6) capable of specific binding with anti-vaccinia virus antibodies (10) present in the fluid test sample (9) to form an immune-complex (1); and
  - a post-filter unit (3) comprising a label zone (7) containing a dried indicator reagent (8), wherein following resolubilization by a buffer reagent (12), said indicator reagent (8) is capable of specifically binding to the immune-complex (1) to produce a visually detectable signal; and wherein the reaction zone (5) of the test unit (2) and the label zone (7) of the post-filter unit (3) are capable of being disposed in transient fluid communication with each other so as to allow direct passage of resolubilized indicator reagent (8) from the label zone (7) into the reaction zone (5) following application of the buffer reagent (12) to the label zone (7).
2. The device (13) according to claim 1, characterized in that the reaction zone (5) comprises a material which has a pore size permitting separation and filtration of unbound components from the fluid test sample (9) and a thickness which permits an adequate amount of purified vaccinia viral lysate (6) to be immobilized thereto.
3. The device (13) according to claim 2, characterized in that the pore size of the material ranges from about 0.1 to 12.0 microns and the thickness of the material ranges from about 0.05 mm to 3.0 mm.
4. The device (13) according to claim 2 or 3, characterized in that non-specific binding sites on a surface of the material are inactivated by application of a protein blocking agent.
5. The device (13) according to any one of claims 2 to 4, characterized in that the material is a nitrocellulose membrane backed with porous paper.
6. The device (13) according to any one of claims 1 to 5, characterized in that the

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vaccinia viral lysate (6) is immobilized within a discrete test zone of the reaction zone (5) by absorption using a dispenser/printer technique.

7. The device (13) according to any one of claims 1 to 6, characterized in that the reaction zone (5) further comprises an immobilized control reagent in a discernable and separate area from the vaccinia viral lysate (6), said control reagent comprising an antibody against a human immunoglobulin selected from the group consisting of IgG, IgM, IgE and IgA.
8. The device (13) according to any one of claims 1 to 7, characterized in that the absorbent zone (4) is separated from the reaction zone (5) by an intervening spacer layer (25) having one or more openings defined therein to permit fluid communication between the reaction zone (5) and the absorbent zone (4).
9. The device (13) according to any one of claims 1 to 8, characterized in that the absorbent zone (4) comprises one or more layers of a wicking material which is capable of wicking fluid by capillary action and absorbing a substantial volume of fluid.
10. The device (13) according to claim 9, characterized in that the wicking material is cellulose acetate.
11. The device (13) according to any one of claims 1 to 10, characterized in that the label zone (7) comprises a filter material having a pore size capable of allowing the dried indicator reagent (8) to be effectively resolubilized by the buffer reagent (12) and transferred to the reaction zone (5) by laminar fluid flow.
12. The device (13) according to claim 11, characterized in that the filter material is glass fiber filter paper.
13. The device (13) according to any one of claims 1 to 12, characterized in that the indicator reagent (8) comprises a direct label.
14. The device (13) according to claim 13, characterized in that the indicator reagent (8) is a colloidal gold-Protein A conjugate.
15. The device (13) according to any one of claims 1 to 14, characterized in that the

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post filter unit (3) is pretreated with a glazing material in the region to which the indicator reagent (8) is applied.

16. The device (13) according any one of claims 1 to 15, characterized in that said test unit (2) and said post-filter unit (3) are contained in a housing.
17. The device (13) according to any one of claims 1 to 16, characterized as further comprising a blood separation zone (100) in lateral communication with the reaction zone (5), wherein the blood separation zone (100) comprises:
  - a first end (101) defining a region for receiving a whole blood test sample (9'), and
  - a second end (102) in direct communication with the reaction zone (5),wherein the blood separation zone comprises a material capable of selectively retaining red blood cells from a whole blood test sample (9') to generate a substantially red blood cell-free fluid portion, and allowing flow of said fluid portion from the first end (101) of the blood separation zone (100) to the reaction zone (5).
18. The device (13) according to claim 17, characterized in that the material capable of selectively retaining red blood cells is a glass fiber material having dimensions between about 4 and 7 mm in width, between about 10 and 15 mm in length and between about 0.2 mm and 1.0 mm in thickness.
19. The device (13) according to claim 17, characterized in that the material capable of selectively retaining red blood cells comprises a hydrophobic carrier or backing (103) capable of reducing seepage of the whole blood test sample (9') and the red blood cell-free fluid portion as it migrates along the blood separation zone (100).
20. The device (13) according to claim 19, characterized in that the hydrophobic carrier or backing (103) is comprised of a material selected from the group consisting of polycarbonate, polyethylene, Mylar™, polypropylene, vinyl, cellophane, polystyrene, water-proofed cardboard and water-resistant cardboard.
21. A method for determining the presence or absence of anti-vaccinia virus antibodies (10) in a fluid test sample (9), characterized by the steps of:

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- depositing the fluid test sample (9) onto the reaction zone (5) of the test unit (2) of a device (13) as defined in any one of claims 1 to 16;
  - bringing the label zone (7) of the post-filter unit (3) and the reaction zone (5) of the test unit (2) into fluid communication therewith;
  - applying a buffer reagent (12) to the post-filter unit (3) to reconstitute the dried indicator reagent (8) and wash any unbound reactants from the reaction zone (5); and
  - removing the post-filter unit (3) to observe a test result depicted by a presence or absence of a visually detectable signal on the reaction zone (5).
22. A method for determining the presence or absence of anti-vaccinia virus antibodies (10) in a whole blood test sample (9'), characterized by the steps of:
- depositing the whole blood test sample (9') onto the first end (101) of the blood separation zone (100) of a device (13) as defined in any one of claims 17 to 20;
  - bringing the label zone (7) of the post-filter unit (3) and the reaction zone (5) of the test unit (2) into fluid communication therewith;
  - applying a buffer reagent (12) to the post-filter unit (3) to reconstitute the dried indicator reagent (8) and wash any unbound reactants from the reaction zone (5); and
  - removing the post-filter unit (3) to observe a test result depicted by a presence or absence of a visually detectable signal on the reaction zone (5).



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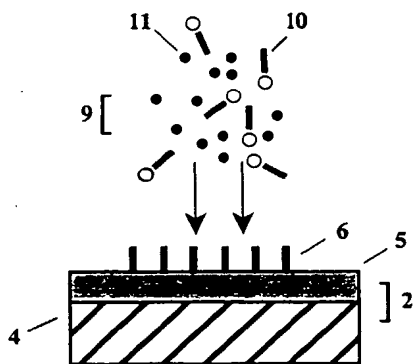


Fig. 1A

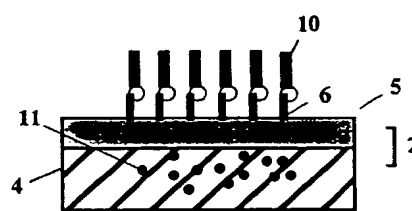


Fig. 1B

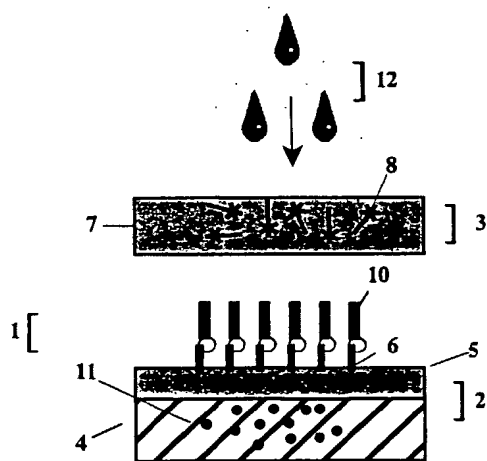


Fig. 1C

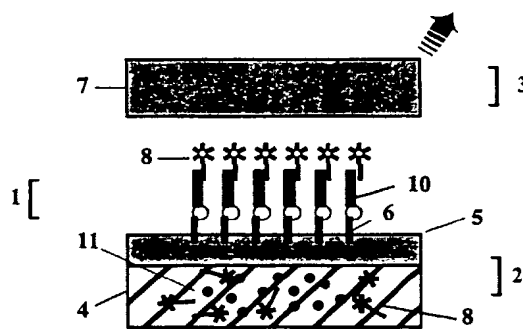


Fig. 1D

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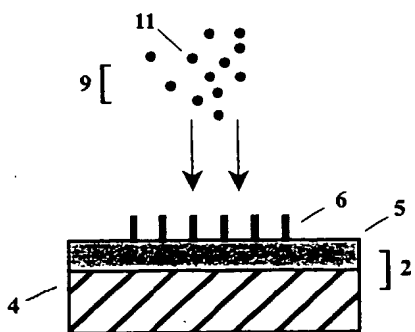


Fig. 2A

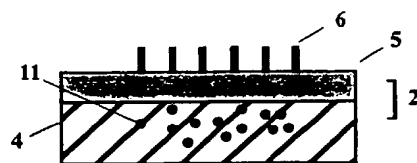


Fig. 2B

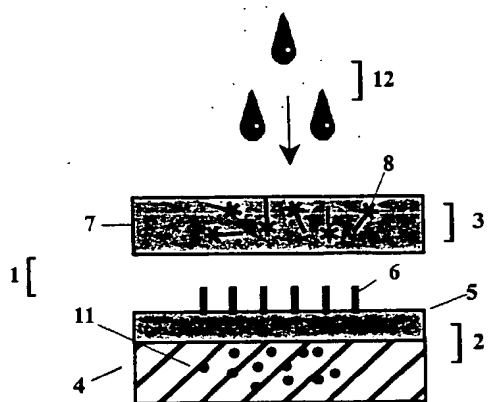


Fig. 2C

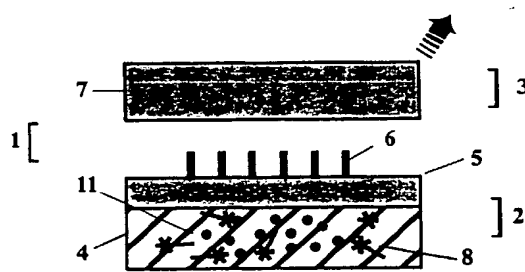
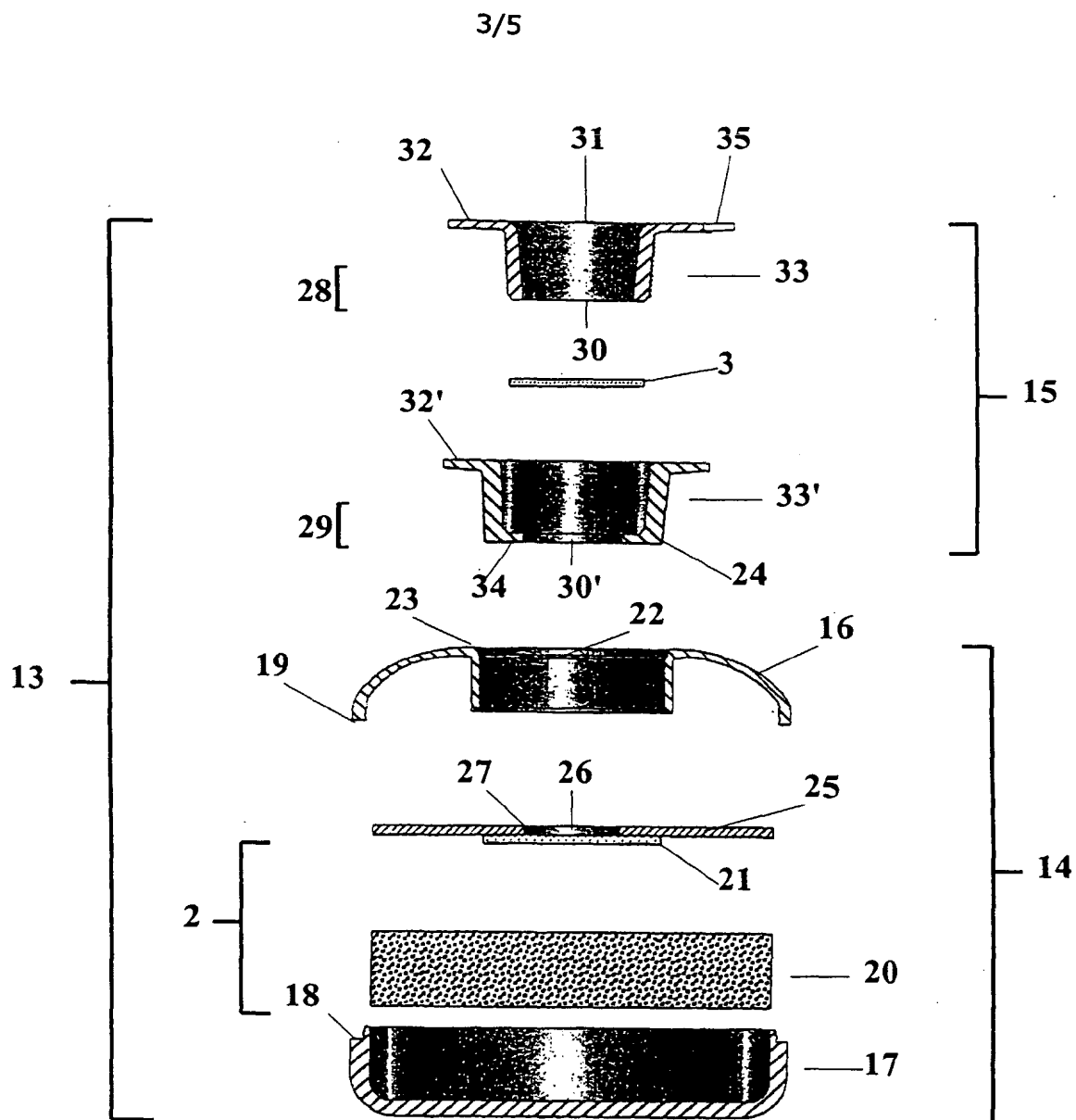


Fig. 2D

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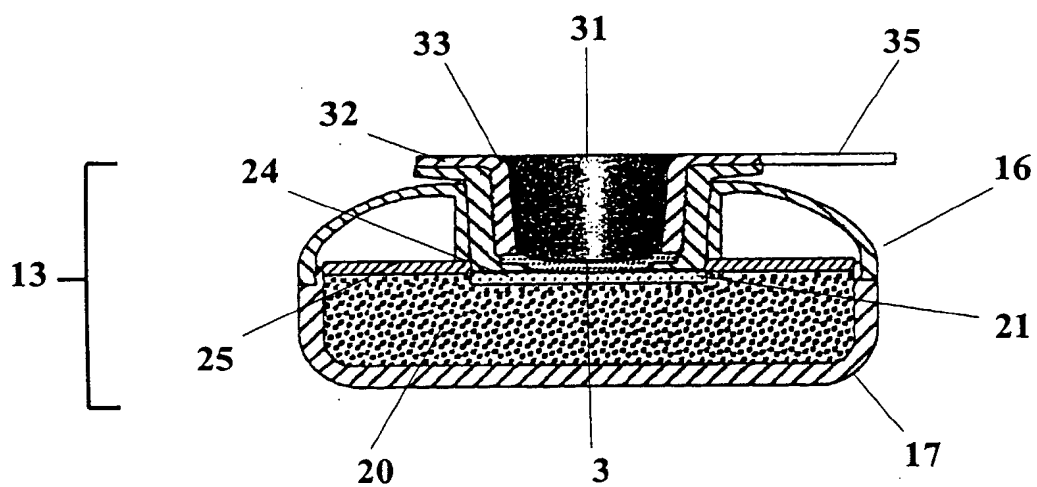


**Fig. 3**

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**Fig. 4**

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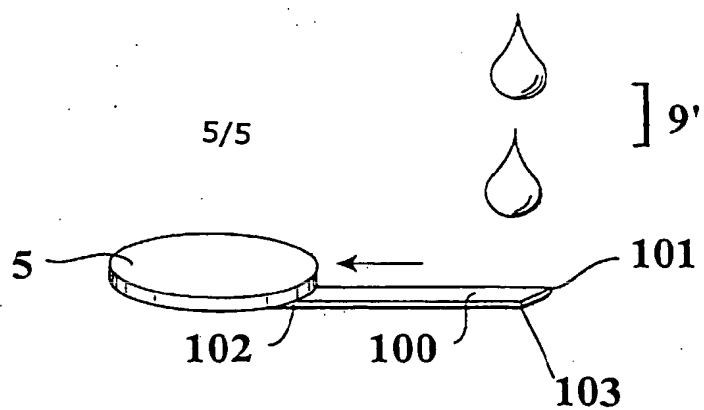


Fig. 5

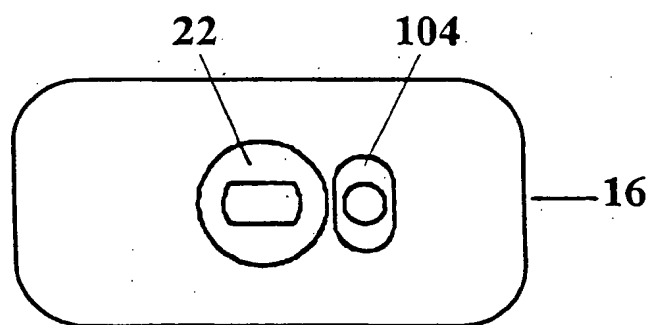


Fig. 6A

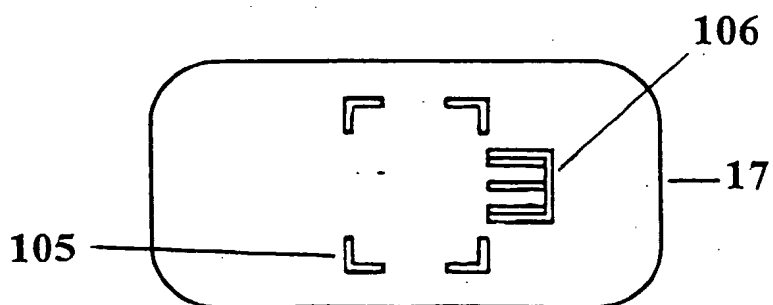


Fig. 6B

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/CA 03/00722

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G01N33/53

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 87 07384 A (QUIDEL) 3 December 1987 (1987-12-03) the whole document ----	1-22
A	EP 0 811 847 A (SECURETEC GMBH ;BOEHRINGER MANNHEIM GMBH (DE)) 10 December 1997 (1997-12-10) the whole document ----	1-22
Y	EP 0 407 904 A (BOEHRINGER MANNHEIM GMBH) 16 January 1991 (1991-01-16) page 5, line 13 - line 20; figure 2 ----	1-22
Y	US 4 965 187 A (TONELLI QUENTIN J) 23 October 1990 (1990-10-23) abstract column 3, line 15 - line 48 figure 1 -----	1-22

☐ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

20 October 2003

Date of mailing of the international search report

30/10/2003

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Information on patent family members

International Application No

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